

# LOCAL ORTHOTROPIC, PLANAR ELASTICITY COMPUTER PROGRAM

|                              |                                                                                     |
|------------------------------|-------------------------------------------------------------------------------------|
| journal or publication title | 国立防災科学技術センター研究速報                                                                    |
| number                       | 59                                                                                  |
| page range                   | 81-137                                                                              |
| year                         | 1984-03-30                                                                          |
| URL                          | <a href="http://id.nii.ac.jp/1625/00002793/">http://id.nii.ac.jp/1625/00002793/</a> |

LOCAL ORTHOTROPIC, PLANAR ELASTICITY COMPUTER PROGRAM

USER MANUAL

PREPARED BY:

THEODORE E. LANG

NATSUO NUMANO

OSAMU ABE

\* \* \* \*

SHINJO BRANCH

NATIONAL RESEARCH CENTER FOR DISASTER PREVENTION

\* \* \* \*

SEPTEMBER 1983

## Contents

|                                                                               | Page    |
|-------------------------------------------------------------------------------|---------|
| Abstract                                                                      | 85      |
| Introduction                                                                  | 86      |
| Plane Stress-Plane Strain                                                     | 87      |
| Triangular and Quadrilateral Elements                                         | 90      |
| Element Stresses                                                              | 90      |
| Program LOPE Structure                                                        | 92      |
| INPUT DATA DESCRIPTION FOR PROGRAM LOPE                                       | 94      |
| Line 1 : Title Data : FORMAT(40A2)                                            | 94      |
| Line 2 : Control Data : FORMAT(5I5, 2F10.0)                                   | 94      |
| Line 3 : Material Data : FORMAT(I5, F10.0, 25A2)                              | 94      |
| Line 4 : Material Coefficients : FORMAT(7E10.4)                               | 95      |
| Line 5 : Nodal Point Data : FORMAT(I5, 3X, 2I1, 5F10.0)                       | 95      |
| Line 6 : Element Data : FORMAT(6I5, F10.0)                                    | 96      |
| Line 7 : Boundary Loading Data : FORMAT(2I5, 2F10.0)                          | 97      |
| OUTPUT DATA                                                                   | 97      |
| Program Operation on Melcom 70                                                | 98      |
| LOPE Test Problem #7                                                          | 100     |
| LOPE Test Problem #8                                                          | 112     |
| LOPE Test Problem #9                                                          | 112     |
| LOPE Test Problem #10                                                         | 117     |
| References                                                                    | 117     |
| APPENDIX    MAIN PROGRAM AND SUBROUTINE LISTING                               | 122-136 |
|                                                                               |         |
| FIGURES AND TABLES                                                            |         |
| FIGURE 1    Node numbering and max. element node difference                   | 88      |
| FIGURE 2    Types of quadrilateral elements                                   | 91      |
| FIGURE 3-1 Element Stresses                                                   | 93      |
| Fig. 3-2                                                                      | 95      |
| Fig. 3-3                                                                      | 96      |
| Fig. 3-4                                                                      | 97      |
| FIGURE 4    Finite Element Representation of Axially Loaded<br>Mild Steel Rod | 101     |
| FIGURE 5    STRESS DISTRIBUTION, TEST PROBLEM #7                              | 103     |
| FIGURE 6    DISPLACEMENT STATE OF UNIFORMLY LOADED ROD                        | 114     |
| FIGURE 7    UNIFORMLY LOADED ROD WITH DISPLACEMENT<br>CONSTRAINT CONDITION    | 115     |
| FIGURE 8    LOADING AND DISPLACEMENT STATE TEST PROBLEM #9                    | 118     |

|                                                                                         | Page |
|-----------------------------------------------------------------------------------------|------|
| TABLE 1    Number of RECORDS necessary for storage of array of<br>bandwidth MBAND       | 99   |
| TABLE 2    INPUT DATA FOR TEST PROBLEM #7                                               | 104  |
| TABLE 3    COMPUTER OUTPUT FOR TEST PROBLEM #7                                          | 105  |
| TABLE 4    COMPUTER INPUT DATA FOR TEST PROBLEM #8                                      | 113  |
| TABLE 5    LISTING OF INPUT DATA FOR TEST PROBLEM #8, WITH<br>A CONSTRAINED NODAL POINT | 116  |
| TABLE 6    INPUT DATA FOR TEST PROBLEM #9                                               | 119  |
| TABLE 7    INPUT DATA FOR TEST PROBLEM #10                                              | 120  |

LOCAL ORTHOTROPIC, PLANAR ELASTICITY COMPUTER PROGRAM

by

THEODORE E. LANG, NATSUO NUMANO and OSAMU ABE

SHINJO BRANCH, NATIONAL RESEARCH CENTER FOR DISASTER PREVENTION  
SHINJO, YAMAGATA-KEN, JAPAN 996

ABSTRACT

Analysis of elasticity and related type problems is facilitated through the development of a finite element (LOPE, Local Orthotropic, Planar Elasticity) code. Direct application is to two-dimensional elasticity problems, that may include material orthotropy, surface and body force loading, and constraint boundary conditions. In addition, the algorithm is applicable to steady state (potential) problems such as in ideal fluid flow, tertiary viscoelastic creep, flow through porous media, and heat transfer. The basic finite element of the code is the constant strain triangular element, which, by superposition, may be used to define quadrilateral shaped elements. The program uses Gauss elimination to solve the set of algebraic equations, which are handled by matrix partitioning in order to accommodate large order problems on medium sized computer systems. The program is operational on the Shinjo Branch (NRCDP) Melcom 70 computer system, and has been used to solve problems where core limits are exceeded. Listing of the computer instructions is given in this reporting, together with input format descriptions, and test problems that check the various options of the program.

### Introduction

A computer code entitled Local Orthotropic, Planar Elasticity (LOPE) has been developed to solve planar elasticity problems by application of the finite element method on the Melcom 70 (Mitsubishi Electric) computer system. Program LOPE is a modified version of program PALOS, originally developed by Goudreau, Nickell and Dunham (1967). Program LOPE is both a simplified and performance improved version of program PALOS. Simplification includes deletion of polar planar geometries, axisymmetric shell geometries, and reduction of options on material and thermal environment representations. Performance is improved by changes in algorithm executions consistent with the functions of the Melcom 70 computer system. Original documentation of program PALOS entitled, "Plane and Axisymmetric Finite Element Analysis of Orthotropic Elastic Solids and Orthotropic Shells", will be considered in this reporting as the primary source on finite element theory pertaining to computer program LOPE. This users manual is intended as a supplement to indicate how input data is formatted for program LOPE, and to provide test problems and statement listings of the code. Anyone using program LOPE is advised to become familiar with the Goudreau, et al. document as may be needed.

Program LOPE may be used to solve planar elasticity problems either in plane-strain or plane-stress, based upon a finite element representation in the plane. Discretization of this plane, designated the x, z plane, into elements may be either triangular or quadrilateral, based upon definition of a set of nodal points interconnected by straight lines. The layout of the element array is an important consideration in making efficient use of the program. One limiting consideration is the spread or difference between node numbers within the individual elements of the problem. The largest difference between node numbers of any element may not exceed 26 in the listed code. Node numbers should be assigned in a regular pattern, and nodes should be numbered across the narrower width of the region. Examples of efficient and

inefficient numbering schemes are shown in Figure 1. After element layout, and nodal numbering, then the maximum node difference in the member can be determined from inspection. Designating this by,  $D_N$ , then the bandwidth of the problem can be defined as

$$MBAND = 2 D_N + 2$$

For the LOPE code, as listed herein,  $D_N \leq 26$ , so that  $MBAND \leq 54$ . Later, use will be made of MBAND in additional calculations. The LOPE code, as listed in the Appendix of this report, has limits expressed in DIMENSION and COMMON statements which are to be considered as a guide, and may be changed as the capacity of the computer permits.

#### Plane Stress-Plane Strain

The general 3-D constitutive law used by the LOPE program allows up to seven material coefficients, namely.

$$\begin{Bmatrix} \sigma_x \\ \sigma_y \\ \sigma_z \\ \tau_{xz} \end{Bmatrix} = \begin{bmatrix} C_{11} & C_{12} & C_{13} & 0 \\ C_{12} & C_{22} & C_{23} & 0 \\ C_{13} & C_{23} & C_{33} & 0 \\ 0 & 0 & 0 & C_{44} \end{bmatrix} \begin{Bmatrix} \epsilon_x \\ \epsilon_y \\ \epsilon_z \\ \gamma_{xz} \end{Bmatrix}$$

To express the C's physically for an isotropic material having material modulus, E, and Poissons ratio,  $\nu$ , we have.

$$C_{11} = C_{22} = C_{33} = \lambda + 2\mu$$

$$C_{12} = C_{13} = C_{23} = \lambda$$

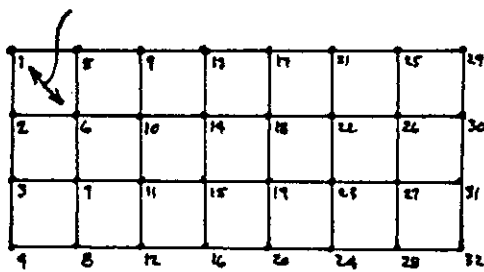
$$C_{44} = \mu$$

where

$$\lambda = \frac{\nu E}{(1+\nu)(1-2\nu)} \quad \mu = \frac{E}{2(1+\nu)}$$

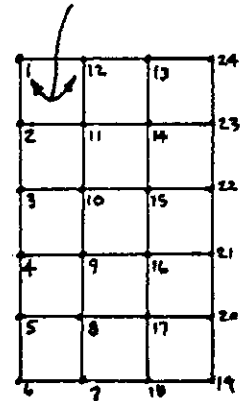
For plane stress in the x, z plane, we set  $\sigma_y = 0$ , which yields  $\epsilon_y = -\frac{C_{23}}{C_{22}} \epsilon_z - \frac{C_{12}}{C_{22}} \epsilon_x$ , which when substituted into the constitutive equations yields

maximum node difference=5



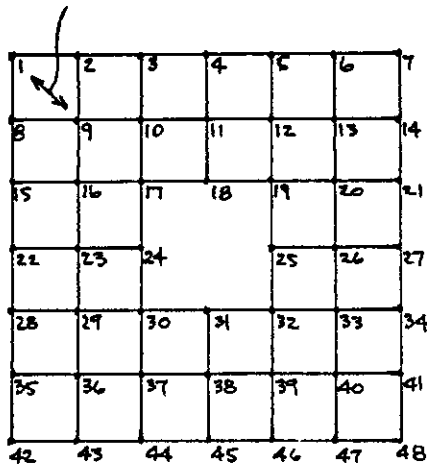
(a) rectangular array-  
efficient numbering

max. node difference=11



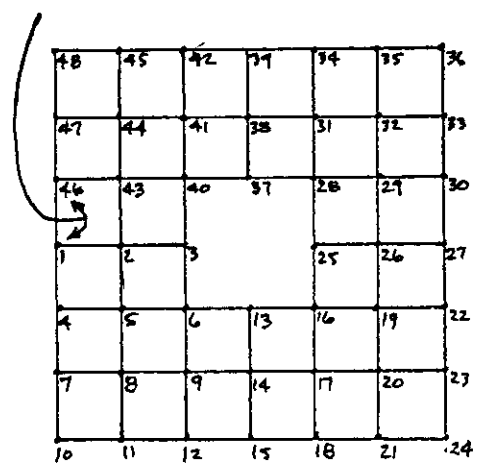
(b) rectangular array-  
inefficient numbering

max. node difference=8



(c) ring array-  
efficient numbering

max. node difference=45



(d) ring array-  
inefficient numbering

Figure 1 : Node numbering and maximum  
element node difference



$$\begin{Bmatrix} \sigma_x \\ \sigma_y \\ \sigma_{xz} \end{Bmatrix} = \begin{bmatrix} C_{11}^* & C_{13}^* & 0 \\ C_{13}^* & C_{33}^* & 0 \\ 0 & 0 & C_{44}^* \end{bmatrix} \begin{Bmatrix} \epsilon_x \\ \epsilon_y \\ \gamma_{xz} \end{Bmatrix}$$

where

$$\begin{aligned} C_{11}^* &= C_{11} - \frac{C_{12}^2}{C_{22}} & C_{33}^* &= C_{33} - \frac{C_{23}^2}{C_{22}} \\ C_{13}^* &= C_{13} - \frac{C_{12}C_{23}}{C_{22}} & C_{44}^* &= C_{44} \end{aligned}$$

The transformation to the  $C^*$ 's is done by the program if  $C_{22}$  is non-zero in the original input array and plane stress is indicated in the input data. If  $C_{22}=0$  then reduction to plane stress is assumed to have been done already with the coefficients that are input. If the program computes the  $C^*$ , then these are output and the plane stress condition is noted.

For plane strain,  $\epsilon_y=0$  and the constitutive law reduces to

$$\begin{Bmatrix} \sigma_x \\ \sigma_y \\ \sigma_z \\ \sigma_{xz} \end{Bmatrix} = \begin{bmatrix} C_{11} & C_{13} & 0 \\ C_{12} & C_{23} & 0 \\ C_{13} & C_{33} & 0 \\ 0 & 0 & C_{44} \end{bmatrix} \begin{Bmatrix} \epsilon_x \\ \epsilon_y \\ \epsilon_z \\ \gamma_{xz} \end{Bmatrix}$$

where no transformation of the  $C$ 's is required.

If the material is orthotropic in the  $x, z$  plane then the seven material constants have different values, and the starting 3D constitutive equation, assuming shear in the  $x, z$  plane, is

$$\begin{Bmatrix} \sigma_x \\ \sigma_y \\ \sigma_z \\ \sigma_{xz} \end{Bmatrix} = \begin{bmatrix} \bar{C}_{11} & \bar{C}_{12} & \bar{C}_{13} & 0 \\ \bar{C}_{12} & \bar{C}_{22} & \bar{C}_{23} & 0 \\ \bar{C}_{13} & \bar{C}_{23} & \bar{C}_{33} & 0 \\ 0 & 0 & 0 & \bar{C}_{44} \end{bmatrix} \begin{Bmatrix} \epsilon_x \\ \epsilon_y \\ \epsilon_z \\ \gamma_{xz} \end{Bmatrix}$$

The inverse of this equation, namely

$$\begin{Bmatrix} \epsilon_x \\ \epsilon_y \\ \epsilon_z \\ \gamma_{xz} \end{Bmatrix} = \begin{bmatrix} A_{11} & A_{12} & A_{13} & 0 \\ A_{12} & A_{22} & A_{23} & 0 \\ A_{13} & A_{23} & A_{33} & 0 \\ 0 & 0 & 0 & A_{44} \end{bmatrix} \begin{Bmatrix} \sigma_x \\ \sigma_y \\ \sigma_z \\ \sigma_{xz} \end{Bmatrix}$$

has the physical meaning  $A_{11} = \frac{1}{E_{11}}$ ,  $A_{22} = \frac{1}{E_{22}}$ ,  $A_{33} = \frac{1}{E_{33}}$

$$A_{12} = -\frac{\nu_{21}}{E_{11}} = -\frac{\nu_{12}}{E_{22}} \quad A_{23} = -\frac{\nu_{32}}{E_{22}} = -\frac{\nu_{23}}{E_{33}}$$

$$A_{13} = -\frac{\nu_{31}}{E_{11}} = -\frac{\nu_{13}}{E_{33}} \quad A_{44} = \frac{1}{G_{12}}$$

Here  $E_{ii}$  is the elastic modulus of the material along the  $i$  axis,

$\nu_{ij} = -\epsilon_{ii}/\epsilon_{jj}$  for stress applied along the  $i$  axis, and  $G_{ij}$  is the shear modulus corresponding to shear stress in the  $i, j$  plane.

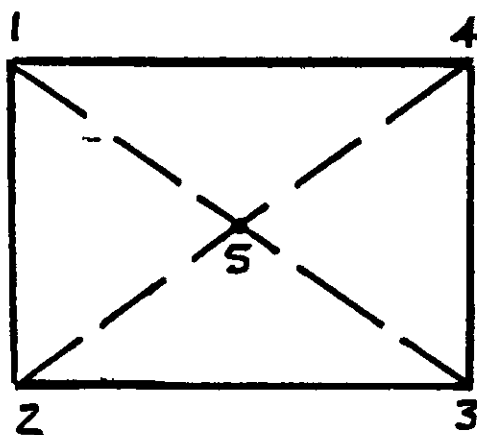
Other interpretations of the C's are required if the computer program is used for steady-state viscoelastic analysis, for steady-state fluid potential flow, or for other planar mechanics problems.

#### Triangular and Quadrilateral Elements

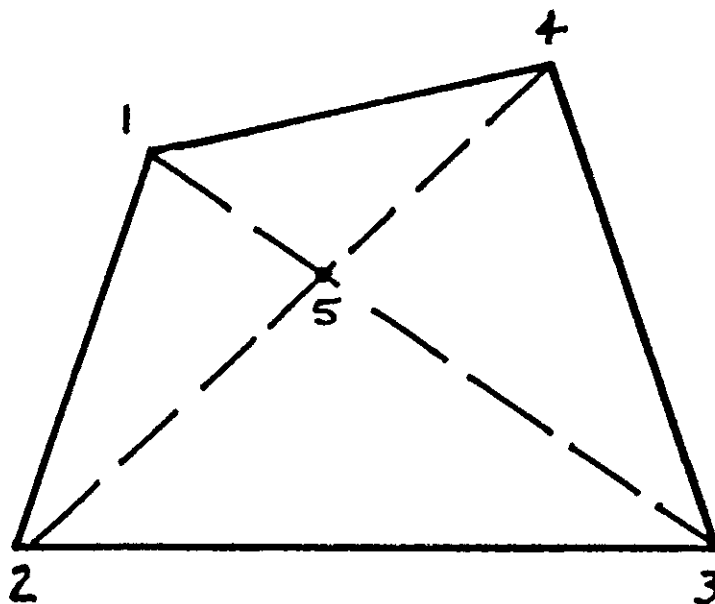
The triangular element used in LOPE is the planar elasticity element commonly reported in finite element texts. The element has 3 nodes, with two displacement components at each node. Thus for the triangular element the stiffness matrix is 6x6. A quadrilateral element, when specified in the input data, is made up from 4 triangular elements by creating a fifth node, which is later deleted from the stiffness matrix. Thus, the final quadrilateral element has 4 nodes, with  $u, v$  displacement components at each node, so that the stiffness matrix is 8x8. The quadrilateral element may be trapezoidal, if necessary (Figure 2).

#### Element Stresses

For each element of a finite element problem one set of stresses is computed, which should be considered as acting at the centroid of the element. In program LOPE several sets of stress components are computed. One set is referenced to the global X, Z coordinate system. These are stresses  $\sigma_{11}$ ,  $\sigma_{33}$  and  $\sigma_{13}$  in Figure 3. A second set of stresses are the principal stresses, which are  $\sigma_{max}$ ,  $\sigma_{min}$  at angle  $\theta$  measured from the X axis (Figure 3). A



(a) regular



(b) trapezoidal

Figure 2 : Types of quadrilateral elements

third set of stresses designated  $\sigma_{nn}$  and  $\sigma_{nt}$  are also computed, which are the stresses normal and tangential to the J, K boundary of the element.

In Figure 3 is also shown the correct sequencing of node numbering consistent with the global coordinate system. If the rotation from the X to Z coordinate axis is counterclockwise, as shown in Figure 3, then the listing of nodes in the element data should also be counterclockwise. Thus, three choices of listing the node points are:

1 - 2 - 3

2 - 3 - 1

3 - 1 - 2

Which one to use depends upon which stress  $\sigma_{JK}$  is desired, and is the choice of the user.

#### Program LOPE Structure

Program LOPE is made up of one MAIN program and four subroutines, named LOCATE, TRISTF, MODULI and MODIFY. Subroutine LOCATE has the purpose of reading and writing program input and control data. Also, several calculations are performed in this subroutine including the interpolation for intermediate nodes and elements that are not listed in the input data, and conversion of pressure boundary conditions to equivalent nodal forces. Number of nodes, elements and matrix bandwidth are also checked relative to limiting values in LOCATE. Subroutine TRISTF is the element stiffness and force vector generation code. It is called once if the element is triangular and four times if the element is quadrilateral. Subroutine MODULI transforms the material coefficient matrix from local to global coordinate reference. Subroutine MODIFY is used to impose displacement boundary conditions on the total structure stiffness matrix. All remaining finite element functions are performed in program MAIN. This includes the following:

1. Element stiffness matrix overlay to form the total structure stiffness

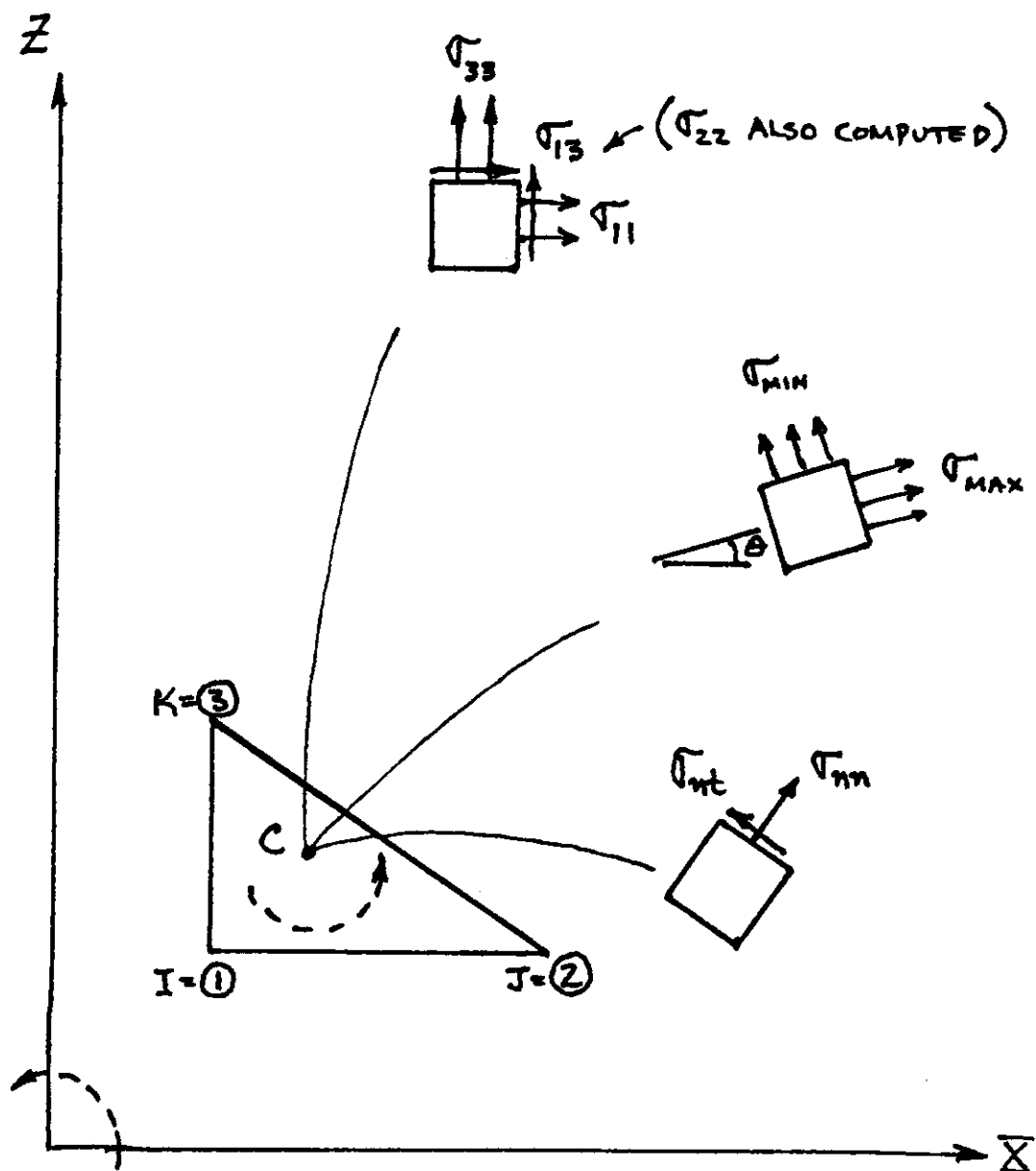


Figure 3-1 : Element Stresses

matrix.

2. Imposition of directional gridpoint displacement conditions.
3. Reduction of the stiffness matrix to semi-diagonal form and back substitution for the displacement solution by Gaussian elimination.
4. Printout of displacements.
5. Calculation and printout of element stresses.

The original PALOS program has proven to be an efficient and useful program to solve 2D elasticity, fluid, and viscoelasticity problems. It is expected that the simplified version, LOPE, has the essential characteristics and utility of the original program.

#### INPUT DATA DESCRIPTION FOR PROGRAM LOPE

##### Line 1 : Title data : FORMAT (40A2)

Columns 1 - 80 : Name and identification information

##### Line 2 : Control Data : FORMAT (5I5, 2F10.0)

Columns 1 - 5 : Number of nodal points (600 maximum)

Columns 6 - 10 : Number of elements (500 maximum)

Columns 11-15 : Number of different materials (10 maximum)

Columns 16-20 : Number of boundary pressure conditions (50 maximum)

Column 25 : Program option:

- 1 plane strain analysis
- 2 plane stress analysis

Columns 26-35 : Acceleration in the X direction

Columns 36-45 : Acceleration in the Z direction

##### Line 3 : Material Data : FORMAT (I5, F10.0, 25A2)

Columns 1 - 5 : Material number (number from 1 to 10)

Columns 6 - 15 : Mass density of the material (this is used only if accelerations are specified, to compute equivalent static force)

Columns 16 - 70 : Material title and identification

Line 4 : Material Coefficients : FORMAT (7E10.4)

|                   | <u>ELASTICITY COEF</u> | <u>ISOTROPIC VALUE</u> |
|-------------------|------------------------|------------------------|
| Columns 1 - 10 :  | $C_{11}$               | $\lambda + 2\mu$       |
| Columns 11 - 20 : | $C_{12}$               | $\lambda$              |
| Columns 21 - 30 : | $C_{13}$               | $\lambda$              |
| Columns 31 - 40 : | $C_{22}$               | $\lambda + 2\mu$       |
| Columns 41 - 50 : | $C_{23}$               | $\lambda$              |
| Columns 51 - 60 : | $C_{33}$               | $\lambda + 2\mu$       |
| Columns 61 - 70 : | $C_{44}$               | $\mu$                  |

All orthotropic material properties are assumed to be defined with respect to the local axes of orthotropy. The Lamé constants  $\lambda$  and  $\mu$  for an isotropic material are related to the engineering constants  $E$  and  $\nu$  by

$$\lambda = \frac{\nu E}{(1+\nu)(1-2\nu)} \quad \mu = \frac{E}{2(1+\nu)}$$

For the case of plane stress ( $\sigma_{yy} = 0$ ) the material coefficients will be modified by the program unless coefficient  $C_{22}$  in columns 31 - 40 is zero, indicating that the coefficients have already been modified.

Line 5 : Nodal Point Data : FORMAT (I5, 3X, 2I1, 5F10.0)

One line is needed for each nodal point (see exception below).

Columns 1 - 5 : Nodal point number

Column 9 : Put 1 if Z displacement is to be specified

Column 10 : Put 1 if X displacement is to be specified

(If columns 9 or 10 are zero or blank, then the corresponding force will be specified).

Columns 11 - 20 : X coordinate of node (in global X, Z)

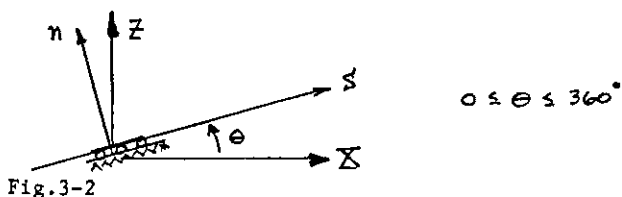
Columns 21 - 30 : Z coordinate of node (in global X, Z)

Columns 31 - 40 : X force or displacement component

Columns 41 - 50 : Z force or displacement component

Columns 51 - 60 : boundary angles (degrees from X axis)

(If a boundary point is constrained to move in a direction S, input the angle, in degrees, from the X axis, positive as shown.



In this case leave columns 9 and 10 blank. Columns 31-40 are then the S force, and columns 41-50 are the displacement).

Nodal points must be listed in numerical sequence. If values are omitted then nodal points are generated at equal intervals along a straight line between the defined nodal points. If the end point boundary codes (9 and 10) are the same at each end of the interval, then that code will be assigned to the generated nodes. If they are different, then the codes will be assigned zero. The generated nodal point forces or displacements will be zero.

Line 6 : Element Data : FORMAT (6I5, F10.0)

One line is needed for each element (see exception below).

Columns 1 - 5 : Element number

Columns 6 - 10 : Nodal point I

Columns 11 - 15 : Nodal point J

Columns 16 - 20 : Nodal point K

Columns 21 - 25 : Nodal point L

Columns 26 - 30 : Material number

Columns 31 - 40 : Local angle of orthotropy (degrees from X axis)

An element may be triangular or quadrilateral, depending upon whether it is defined by three or four nodes, respectively. If the global axes transform from the X to Z axis by a counterclockwise rotation, then the nodal sequence I-J-K-L must be a counterclockwise rotation around the element. If the element is triangular, set L=K.

The maximum difference between any pair of I, J, K, L may not exceed 26 (the maximum node numbering difference of the problem).

If the principal material axes  $\bar{x}$ ,  $\bar{z}$  of an orthotropic material element are different from the global X, Z axes, then the angle (in degrees) from the X axis is input positive as shown.

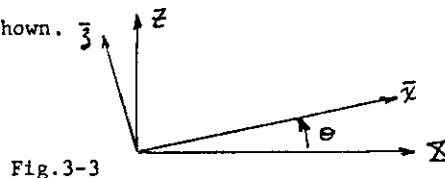


Fig.3-3



Elements must be listed in numerical sequence. If element numbers are omitted, then elements are generated by incrementing I, J, K and L of the previous element by one. The material identification code and the local angle of orthotropy are set equal to that of the previous line. The last element of the problem must always be input.

Line 7 : Boundary Loading Data : FORMAT (2I5, 2F10.0)

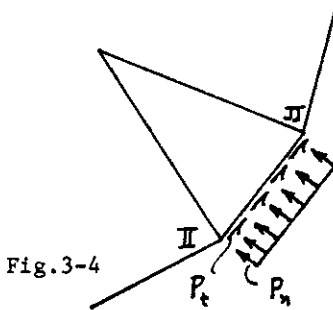
One line is needed for each boundary segment which is subjected to a normal or tangential pressure.

Columns 1 - 5 : Nodal point II

Columns 6 - 10 : Nodal point JJ

Columns 11 - 20 : Normal Pressure

Columns 21 - 30 : Tangential Pressure



The boundary element must be on the left as one progresses from II to JJ. Surface tensile force is input as a negative pressure. Positive shear pressure is in the direction from II to JJ.

OUTPUT DATA

The following information is output from the computer.

1. Printout of the input data. If, in a plane stress problem the material coefficients are modified, then the modified set are output. The program also outputs whether the plane stress or plane strain option is being used.
2. Printout of the computed node point displacements.
3. Printout of the centroidal stresses and strains in the following coordinate systems:
  - A. global
  - B. principal (with separate angle for stresses and strains)
  - C. Normal and tangential to J-K face

(see Figure 3 for further definition of the stress components)

### Program Operation on Melcom 70

The original main program and three levels of eight subroutines comprised in program PALOS, were replaced by a main program and one level of four subroutines in program LOPE. The main program in LOPE was expanded to include three of the longest subroutines in program PALOS. The remaining 5 subroutines were reduced to 4 and accessed at one level of subroutine entry, as required by the Melcom 70 system. One data storage and access option in program PALOS that provides efficient data handling, was simulated in program LOPE in order to retain the same efficiency. The option takes into account the array symmetry and band limiting characteristics of the finite element stiffness matrix. In stiffness matrix generation and overlay only the lower diagonal and off-diagonal elements are retained, and these data are generated, stored and re-read from computer memory, to disk, and back into memory by blocks. This process of data handling is efficient relative to total storage allocation needed in problem execution on the Melcom 70 system. A user of the program, in taking advantage of this data handling feature must make some simple preliminary calculations prior to assigning disk storage for program execution.

A BLOCK of data is defined, using the bandwidth (MBAND) defined earlier, as

$$\text{BLOCK OF DATA} = \text{DATA LENGTH} = (\text{MBAND} + 1) \times 54$$

There may be several BLOCKS OF DATA, the number of which may be computed as follows

$$\text{NO. OF BLOCKS} = \frac{\text{MAXIMUM NODE NUMBER OF GRID}}{27}$$

rounded off to the next larger whole number (integer). On the Melcom 70 the record length on the computer disks is defined as

$$\text{RECORD LENGTH (2D DISK)} = 256 \text{ bytes} = 128 \text{ words}$$

for an unformatted R/W statement. However, two words are needed to store each REAL NUMBER of a data set. Thus, the number of RECORDS needed for each BLOCK

OF DATA may be computed based upon the value of the bandwidth (MBAND). The result of this computation is summarized in Table 1.

TABLE 1 : Number of RECORDS necessary for storage of array of bandwidth MBAND

| MBAND | DATA LENGTH | NO. OF RECORDS/BLOCK |
|-------|-------------|----------------------|
| 4     | 270         | 5                    |
| 6     | 378         | 6                    |
| 8     | 486         | 8                    |
| 10    | 594         | 10                   |
| 12    | 702         | 11                   |
| 14    | 810         | 13                   |
| 16    | 918         | 15                   |
| 18    | 1026        | 17                   |
| 20    | 1134        | 18                   |
| 22    | 1242        | 20                   |
| 24    | 1350        | 22                   |
| 26    | 1458        | 23                   |
| 28    | 1566        | 25                   |
| 30    | 1674        | 27                   |
| 32    | 1782        | 28                   |
| 34    | 1890        | 30                   |
| 36    | 1998        | 32                   |
| 38    | 2106        | 33                   |
| 40    | 2214        | 35                   |
| 42    | 2322        | 37                   |
| 44    | 2430        | 38                   |
| 46    | 2538        | 40                   |
| 48    | 2646        | 42                   |
| 50    | 2754        | 44                   |
| 52    | 2862        | 45                   |
| 54    | 2970        | 47                   |

In summary, once the bandwidth (MBAND) is known, then from Table 1 the NO. OF RECORDS/BLOCK can be determined, finally multiplying by the NO. OF BLOCKS, as computed above, yields the total NO. OF RECORDS needed for the problem being solved. This number is used to define disk storage, and if designated STORE, the format of the statement is

@@// DEFIN UD, STORE, NO. OF RECORDS, U

Following this, DEVICE no. 11 is specified in program LOPE so an assign statement (ASGN) is needed of the form

```
00 // ASGN U11 = STORE, UD
```

Assuming that a problem data file has been built, designated DATA, then the sequence of computer instructions needed to execute (EXEC) a problem is:

```
00 // ASGN U7 = DATA, UD
```

```
00 // DEF1 UD, STORE, NO. OF RECORDS, U
```

```
00 // ASGN U11 = STORE, UD
```

```
00 // EXEC LOPE, UD
```

These instructions assume that data area UD is used and that the LOPE program has been compiled and placed in disk area UD.

#### LOPE Test Problem #7

This test problem is designed to check the basic operations in program LOPE, including INPUT-OUTPUT, DISPLACEMENT COMPUTATION and ELEMENT STRESS COMPUTATION. In addition, the problem is large enough that three BLOCKS of data are generated, of which two are stored on disk by the WRITE-READ-  
BACKSPACE function on the Melcom 70 computer.

The test problem is of an axial rod of mild steel supported at one end ( $X=0$ ) and loaded by a concentrated force of 10,000 LB at the other end ( $X=10''$ ). The finite element representation of the problem uses 40 square elements that are 1" by 1", with corresponding 55 nodal points (Figure 4). The 10,000 LB load acts in the positive X direction, and is applied at node point #53 (Figure 4). The axial rod is assumed 1" in the third dimension, otherwise the 10,000 LB force may require redefinition. At the upper (supported) end of the axial rod displacements  $U_1, U_2, U_3, U_4, U_5$  in the X direction are set to zero. However in the Z direction the rod is allowed to change width, as only  $U_3=0$ . These displacement constraints at the supported end of the rod are sufficient to prevent any rigid body translation

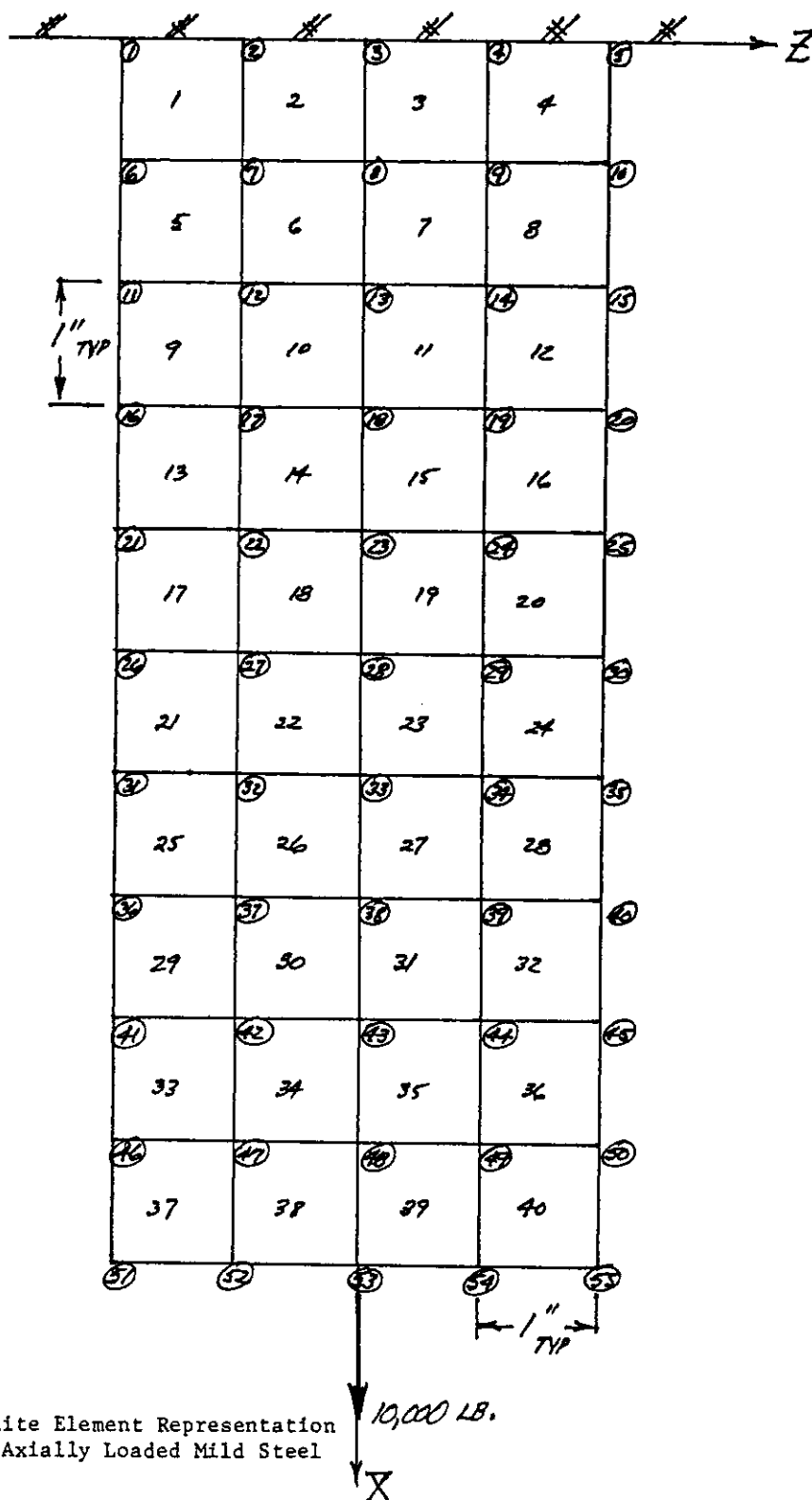


Figure 4 : Finite Element Representation of Axially Loaded Mild Steel Rod

in the X-Z plane, or rotation about the Y axis, which always must be checked. If rigid body motions are not prevented, then the solution returned by LOPE will not be well-defined.

Another reason for selection of the test problem above, is that a closed form solution for the stresses in the rod are given by Timoshenko (1970), which can be compared with the program computed values. The comparison is shown in Figure 5 at three stations along the rod,  $X=6.0''$ ,  $8.0''$  and  $9.0''$ . The solid line distribution is that reported by Timoshenko, and the X values are the values obtained from the computer solution. A close correspondance between the two sets of values is evident, and by making the finite element grid finer, more finite element stresses can be computed across the width of the rod.

The input data for this problem is listed in Table 2, and the computer output is listed in Table 3.

Figure 5 : STRESS DISTRIBUTION, TEST PROBLEM #7

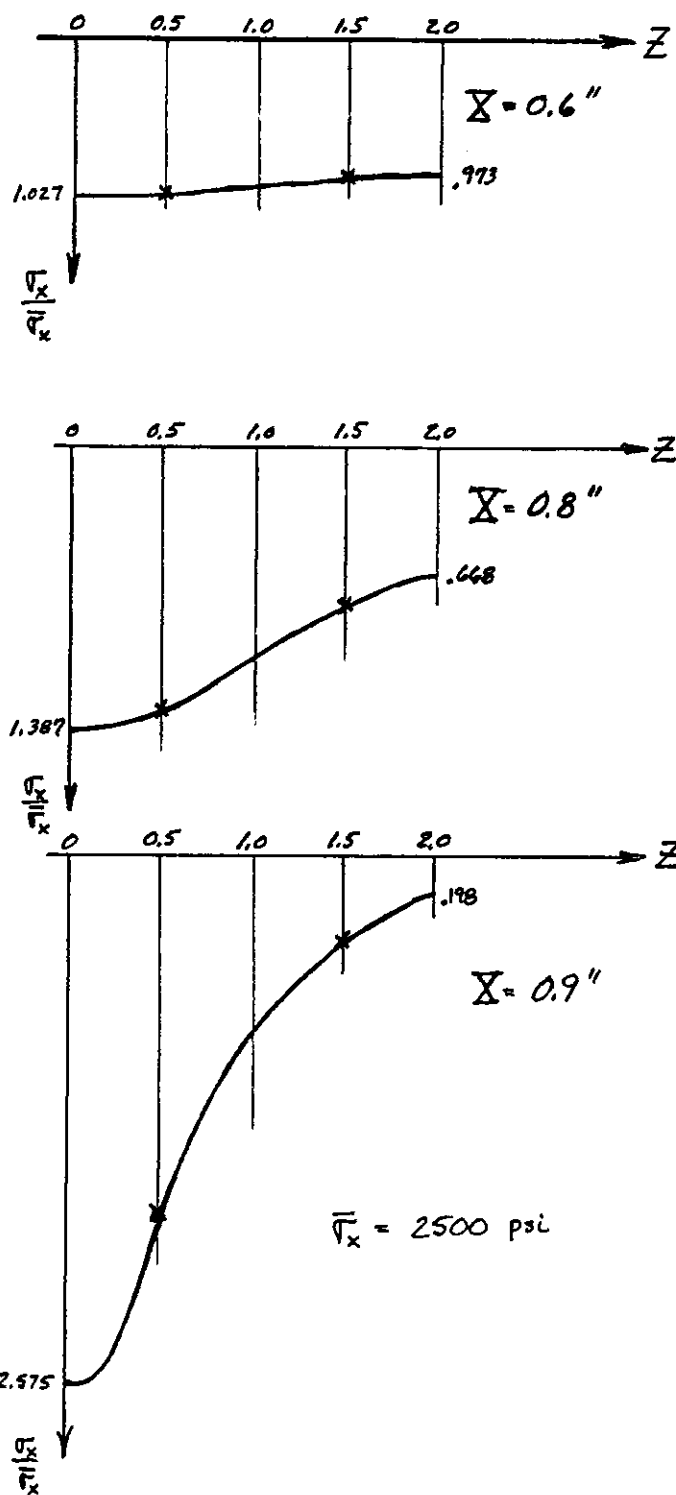


TABLE 2 : INPUT DATA FOR TEST PROBLEM #7

| LOPE TEST PROBLEM #7 |          |    |          |      |          |          |          |          |          |  |  |
|----------------------|----------|----|----------|------|----------|----------|----------|----------|----------|--|--|
| 1                    |          |    |          |      |          |          |          |          |          |  |  |
| 2                    | 55       | 40 | 1        | 0    | 2        | 0.0      | 0.0      |          |          |  |  |
| 3                    | 1        |    | 0.0      |      |          |          |          |          |          |  |  |
| 4                    | .403 E08 |    | .173 E08 |      | .173 E08 | .403 E08 | .173 E08 | .403 E08 | .115 E08 |  |  |
| 5                    | 1        | 1  |          | 0.0  | -2.0     | 0.0      |          |          |          |  |  |
| 6                    | 2        | 1  |          | 0.0  | -1.0     | 0.0      |          |          |          |  |  |
| 7                    | 3        | 11 |          | 0.0  | 0.0      | 0.0      | 0.0      |          |          |  |  |
| 8                    | 4        | 1  |          | 0.0  | 1.0      | 0.0      |          |          |          |  |  |
| 9                    | 5        | 1  |          | 0.0  | 2.0      | 0.0      |          |          |          |  |  |
| 10                   | 6        |    |          | 1.0  | -2.0     |          |          |          |          |  |  |
| 11                   | 10       |    |          | 1.0  | 2.0      |          |          |          |          |  |  |
| 12                   | 11       |    |          | 2.0  | -2.0     |          |          |          |          |  |  |
| 13                   | 15       |    |          | 2.0  | 2.0      |          |          |          |          |  |  |
| 14                   | 16       |    |          | 3.0  | -2.0     |          |          |          |          |  |  |
| 15                   | 20       |    |          | 3.0  | 2.0      |          |          |          |          |  |  |
| 16                   | 21       |    |          | 4.0  | -2.0     |          |          |          |          |  |  |
| 17                   | 25       |    |          | 4.0  | 2.0      |          |          |          |          |  |  |
| 18                   | 26       |    |          | 5.0  | -2.0     |          |          |          |          |  |  |
| 19                   | 30       |    |          | 5.0  | 2.0      |          |          |          |          |  |  |
| 20                   | 31       |    |          | 6.0  | -2.0     |          |          |          |          |  |  |
| 21                   | 35       |    |          | 6.0  | 2.0      |          |          |          |          |  |  |
| 22                   | 36       |    |          | 7.0  | -2.0     |          |          |          |          |  |  |
| 23                   | 40       |    |          | 7.0  | 2.0      |          |          |          |          |  |  |
| 24                   | 41       |    |          | 8.0  | -2.0     |          |          |          |          |  |  |
| 25                   | 45       |    |          | 8.0  | 2.0      |          |          |          |          |  |  |
| 26                   | 46       |    |          | 9.0  | -2.0     |          |          |          |          |  |  |
| 27                   | 50       |    |          | 9.0  | 2.0      |          |          |          |          |  |  |
| 28                   | 51       |    |          | 10.0 | -2.0     |          |          |          |          |  |  |
| 29                   | 52       |    |          | 10.0 | -1.0     |          |          |          |          |  |  |
| 30                   | 53       |    |          | 10.0 | 0.0      | 10000    |          |          |          |  |  |
| 31                   | 54       |    |          | 10.0 | 1.0      |          |          |          |          |  |  |
| 32                   | 55       |    |          | 10.0 | 2.0      |          |          |          |          |  |  |
| 33                   | 1        | 1  | 6        | 7    | 2        | 1        |          |          |          |  |  |
| 34                   | 5        | 6  | 11       | 12   | 7        | 1        |          |          |          |  |  |
| 35                   | 9        | 11 | 16       | 17   | 12       | 1        |          |          |          |  |  |
| 36                   | 13       | 16 | 21       | 22   | 17       | 1        |          |          |          |  |  |
| 37                   | 17       | 21 | 26       | 27   | 22       | 1        |          |          |          |  |  |
| 38                   | 21       | 26 | 31       | 32   | 27       | 1        |          |          |          |  |  |
| 39                   | 25       | 31 | 36       | 37   | 32       | 1        |          |          |          |  |  |
| 40                   | 29       | 36 | 41       | 42   | 37       | 1        |          |          |          |  |  |
| 41                   | 33       | 41 | 46       | 47   | 42       | 1        |          |          |          |  |  |
| 42                   | 37       | 46 | 51       | 52   | 47       | 1        |          |          |          |  |  |
| 43                   | 40       | 49 | 54       | 55   | 50       | 1        |          |          |          |  |  |



TABLE 3 : COMPUTER OUTPUT FOR TEST PROBLEM #7

- PAGE 1 -

LOPE TEST PROBLEM #7

PLANE STRESS PROBLEM

|                                   |            |
|-----------------------------------|------------|
| NUMBER OF NODAL POINTS-----       | 55         |
| NUMBER OF ELEMENTS-----           | 40         |
| NUMBER OF DIFFERENT MATERIALS---  | 1          |
| NUMBER OF PRES/SHEAR CONDITIONS-- | 0          |
| X1 ACCELERATION-----              | 0.0000E-01 |
| X3 ACCELERATION-----              | 0.0000E-01 |

- PAGE 2 -

MATERIAL DATA

|   |                                       |          |      |          |      |          |          |          |
|---|---------------------------------------|----------|------|----------|------|----------|----------|----------|
| 1 | MILD STEEL                            |          |      |          |      |          |          |          |
|   | C11=                                  | 4.03E+07 | C12= | 1.73E+07 | C13= | 1.73E+07 | C22=     | 4.03E+07 |
|   | C23=                                  | 1.73E+07 | C33= | 4.03E+07 | C44= | 1.15E+07 | DENSITY= | 0.00E-01 |
|   | PLANE STRESS REDUCTION OF MATR. COEF. |          |      |          |      |          |          |          |
|   | C11=                                  | 3.29E+07 | C12= | 0.00E-01 | C13= | 9.87E+06 | C22=     | 0.00E-01 |
|   | C23=                                  | 0.00E-01 | C33= | 3.29E+07 | C44= | 1.15E+07 | DENSITY= | 0.00E-01 |

- PAGE 3 -

| NODE PNT | CODE | X1-COORD | X3-COORD | X1-LD OR DISP | X3-LD OR DISP | ANGLE      |
|----------|------|----------|----------|---------------|---------------|------------|
| 1        | 1.   | 0.0000   | -2.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 2        | 1.   | 0.0000   | -1.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 3        | 11.  | 0.0000   | 0.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 4        | 1.   | 0.0000   | 1.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 5        | 1.   | 0.0000   | 2.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 6        | 0.   | 1.0000   | -2.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 7        | 0.   | 1.0000   | -1.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 8        | 0.   | 1.0000   | 0.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 9        | 0.   | 1.0000   | 1.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 10       | 0.   | 1.0000   | 2.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 11       | 0.   | 2.0000   | -2.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 12       | 0.   | 2.0000   | -1.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 13       | 0.   | 2.0000   | 0.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 14       | 0.   | 2.0000   | 1.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 15       | 0.   | 2.0000   | 2.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 16       | 0.   | 3.0000   | -2.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 17       | 0.   | 3.0000   | -1.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 18       | 0.   | 3.0000   | 0.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 19       | 0.   | 3.0000   | 1.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 20       | 0.   | 3.0000   | 2.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 21       | 0.   | 4.0000   | -2.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 22       | 0.   | 4.0000   | -1.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 23       | 0.   | 4.0000   | 0.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 24       | 0.   | 4.0000   | 1.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 25       | 0.   | 4.0000   | 2.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 26       | 0.   | 5.0000   | -2.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 27       | 0.   | 5.0000   | -1.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 28       | 0.   | 5.0000   | 0.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 29       | 0.   | 5.0000   | 1.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 30       | 0.   | 5.0000   | 2.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 31       | 0.   | 6.0000   | -2.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 32       | 0.   | 6.0000   | -1.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 33       | 0.   | 6.0000   | 0.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 34       | 0.   | 6.0000   | 1.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 35       | 0.   | 6.0000   | 2.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 36       | 0.   | 7.0000   | -2.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 37       | 0.   | 7.0000   | -1.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 38       | 0.   | 7.0000   | 0.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 39       | 0.   | 7.0000   | 1.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 40       | 0.   | 7.0000   | 2.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 41       | 0.   | 8.0000   | -2.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 42       | 0.   | 8.0000   | -1.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 43       | 0.   | 8.0000   | 0.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 44       | 0.   | 8.0000   | 1.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 45       | 0.   | 8.0000   | 2.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 46       | 0.   | 9.0000   | -2.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 47       | 0.   | 9.0000   | -1.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 48       | 0.   | 9.0000   | 0.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 49       | 0.   | 9.0000   | 1.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 50       | 0.   | 9.0000   | 2.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 51       | 0.   | 10.0000  | -2.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 52       | 0.   | 10.0000  | -1.0000  | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 53       | 0.   | 10.0000  | 0.0000   | 1.0000E+04    | 0.0000E-01    | 0.0000E-01 |
| 54       | 0.   | 10.0000  | 1.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |
| 55       | 0.   | 10.0000  | 2.0000   | 0.0000E-01    | 0.0000E-01    | 0.0000E-01 |

- PAGE 4 -

| ELEMENT | I  | J  | K  | L  | MATERIAL | ANGLE      |
|---------|----|----|----|----|----------|------------|
| 1       | 1  | 6  | 7  | 2  | 1        | 0.0000E-01 |
| 2       | 2  | 7  | 8  | 3  | 1        | 0.0000E-01 |
| 3       | 3  | 8  | 9  | 4  | 1        | 0.0000E-01 |
| 4       | 4  | 9  | 10 | 5  | 1        | 0.0000E-01 |
| 5       | 6  | 11 | 12 | 7  | 1        | 0.0000E-01 |
| 6       | 7  | 12 | 13 | 8  | 1        | 0.0000E-01 |
| 7       | 8  | 13 | 14 | 9  | 1        | 0.0000E-01 |
| 8       | 9  | 14 | 15 | 10 | 1        | 0.0000E-01 |
| 9       | 11 | 16 | 17 | 12 | 1        | 0.0000E-01 |
| 10      | 12 | 17 | 18 | 13 | 1        | 0.0000E-01 |
| 11      | 13 | 18 | 19 | 14 | 1        | 0.0000E-01 |
| 12      | 14 | 19 | 20 | 15 | 1        | 0.0000E-01 |
| 13      | 16 | 21 | 22 | 17 | 1        | 0.0000E-01 |
| 14      | 17 | 22 | 23 | 18 | 1        | 0.0000E-01 |
| 15      | 18 | 23 | 24 | 19 | 1        | 0.0000E-01 |
| 16      | 19 | 24 | 25 | 20 | 1        | 0.0000E-01 |
| 17      | 21 | 26 | 27 | 22 | 1        | 0.0000E-01 |
| 18      | 22 | 27 | 28 | 23 | 1        | 0.0000E-01 |
| 19      | 23 | 28 | 29 | 24 | 1        | 0.0000E-01 |
| 20      | 24 | 29 | 30 | 25 | 1        | 0.0000E-01 |
| 21      | 26 | 31 | 32 | 27 | 1        | 0.0000E-01 |
| 22      | 27 | 32 | 33 | 28 | 1        | 0.0000E-01 |
| 23      | 28 | 33 | 34 | 29 | 1        | 0.0000E-01 |
| 24      | 29 | 34 | 35 | 30 | 1        | 0.0000E-01 |
| 25      | 31 | 36 | 37 | 32 | 1        | 0.0000E-01 |
| 26      | 32 | 37 | 38 | 33 | 1        | 0.0000E-01 |
| 27      | 33 | 38 | 39 | 34 | 1        | 0.0000E-01 |
| 28      | 34 | 39 | 40 | 35 | 1        | 0.0000E-01 |
| 29      | 36 | 41 | 42 | 37 | 1        | 0.0000E-01 |
| 30      | 37 | 42 | 43 | 38 | 1        | 0.0000E-01 |
| 31      | 38 | 43 | 44 | 39 | 1        | 0.0000E-01 |
| 32      | 39 | 44 | 45 | 40 | 1        | 0.0000E-01 |
| 33      | 41 | 46 | 47 | 42 | 1        | 0.0000E-01 |
| 34      | 42 | 47 | 48 | 43 | 1        | 0.0000E-01 |
| 35      | 43 | 48 | 49 | 44 | 1        | 0.0000E-01 |
| 36      | 44 | 49 | 50 | 45 | 1        | 0.0000E-01 |
| 37      | 46 | 51 | 52 | 47 | 1        | 0.0000E-01 |
| 38      | 47 | 52 | 53 | 48 | 1        | 0.0000E-01 |
| 39      | 48 | 53 | 54 | 49 | 1        | 0.0000E-01 |
| 40      | 49 | 54 | 55 | 50 | 1        | 0.0000E-01 |

BANDWIDTH----- 14

- PAGE 5 -

| NP | X1    | X3    | U1         | U3          |
|----|-------|-------|------------|-------------|
| 1  | 0.00  | -2.00 | 0.0000E-01 | 5.0207E-05  |
| 2  | 0.00  | -1.00 | 0.0000E-01 | 2.5101E-05  |
| 3  | 0.00  | 0.00  | 0.0000E-01 | 0.0000E-01  |
| 4  | 0.00  | 1.00  | 0.0000E-01 | -2.5099E-05 |
| 5  | 0.00  | 2.00  | 0.0000E-01 | -5.0204E-05 |
| 6  | 1.00  | -2.00 | 8.3599E-05 | 5.0186E-05  |
| 7  | 1.00  | -1.00 | 8.3609E-05 | 2.5083E-05  |
| 8  | 1.00  | 0.00  | 8.3600E-05 | 2.1109E-09  |
| 9  | 1.00  | 1.00  | 8.3609E-05 | -2.5079E-05 |
| 10 | 1.00  | 2.00  | 8.3597E-05 | -5.0182E-05 |
| 11 | 2.00  | -2.00 | 1.6724E-04 | 5.0119E-05  |
| 12 | 2.00  | -1.00 | 1.6721E-04 | 2.5024E-05  |
| 13 | 2.00  | 0.00  | 1.6715E-04 | 3.6198E-09  |
| 14 | 2.00  | 1.00  | 1.6721E-04 | -2.5017E-05 |
| 15 | 2.00  | 2.00  | 1.6724E-04 | -5.0111E-05 |
| 16 | 3.00  | -2.00 | 2.5103E-04 | 5.0037E-05  |
| 17 | 3.00  | -1.00 | 2.5077E-04 | 2.4936E-05  |
| 18 | 3.00  | 0.00  | 2.5057E-04 | 5.3124E-09  |
| 19 | 3.00  | 1.00  | 2.5077E-04 | -2.4926E-05 |
| 20 | 3.00  | 2.00  | 2.5102E-04 | -5.0027E-05 |
| 21 | 4.00  | -2.00 | 3.3518E-04 | 5.0195E-05  |
| 22 | 4.00  | -1.00 | 3.3426E-04 | 2.5006E-05  |
| 23 | 4.00  | 0.00  | 3.3380E-04 | 6.9440E-09  |
| 24 | 4.00  | 1.00  | 3.3426E-04 | -2.4992E-05 |
| 25 | 4.00  | 2.00  | 3.3517E-04 | -5.0181E-05 |
| 26 | 5.00  | -2.00 | 4.1984E-04 | 5.1502E-05  |
| 27 | 5.00  | -1.00 | 4.1767E-04 | 2.5971E-05  |
| 28 | 5.00  | 0.00  | 4.1711E-04 | 6.3810E-09  |
| 29 | 5.00  | 1.00  | 4.1767E-04 | -2.5954E-05 |
| 30 | 5.00  | 2.00  | 4.1983E-04 | -5.1485E-05 |
| 31 | 6.00  | -2.00 | 5.0406E-04 | 5.6130E-05  |
| 32 | 6.00  | -1.00 | 5.0129E-04 | 2.9730E-05  |
| 33 | 6.00  | 0.00  | 5.0223E-04 | 9.4224E-09  |
| 34 | 6.00  | 1.00  | 5.0128E-04 | -2.9711E-05 |
| 35 | 6.00  | 2.00  | 5.0406E-04 | -5.6112E-05 |
| 36 | 7.00  | -2.00 | 5.8258E-04 | 6.6783E-05  |
| 37 | 7.00  | -1.00 | 5.8625E-04 | 3.9316E-05  |
| 38 | 7.00  | 0.00  | 5.9494E-04 | 1.0053E-08  |
| 39 | 7.00  | 1.00  | 5.8625E-04 | -3.9296E-05 |
| 40 | 7.00  | 2.00  | 5.8258E-04 | -6.6763E-05 |
| 41 | 8.00  | -2.00 | 6.3950E-04 | 8.0572E-05  |
| 42 | 8.00  | -1.00 | 6.7532E-04 | 5.3509E-05  |
| 43 | 8.00  | 0.00  | 7.0836E-04 | 1.0617E-08  |
| 44 | 8.00  | 1.00  | 6.7532E-04 | -5.3488E-05 |
| 45 | 8.00  | 2.00  | 6.3950E-04 | -8.0551E-05 |
| 46 | 9.00  | -2.00 | 6.4661E-04 | 4.9492E-05  |
| 47 | 9.00  | -1.00 | 7.5939E-04 | 5.8812E-05  |
| 48 | 9.00  | 0.00  | 8.7538E-04 | 1.1197E-08  |
| 49 | 9.00  | 1.00  | 7.5939E-04 | -5.8790E-05 |
| 50 | 9.00  | 2.00  | 6.4661E-04 | -4.9470E-05 |
| 51 | 10.00 | -2.00 | 6.4642E-04 | -5.5701E-05 |
| 52 | 10.00 | -1.00 | 7.5892E-04 | -5.7425E-05 |
| 53 | 10.00 | 0.00  | 1.1799E-03 | 1.1411E-08  |
| 54 | 10.00 | 1.00  | 7.5892E-04 | 5.7448E-05  |
| 55 | 10.00 | 2.00  | 6.4642E-04 | 5.5724E-05  |

- PAGE 6 -

| ELM | X1<br>MATERIAL | X3    | 1-STRESS<br>1-STRAIN   | 2-STRESS<br>2-STRAIN   | 3-STRESS<br>3-STRAIN    | 13-STRESS<br>13-STRAIN   | MAX-STRESS<br>MAX-STRAIN | MIN-STRESS<br>MIN-STRAIN | ANGLE          | JK-STRESS<br>JK-SHEAR   |
|-----|----------------|-------|------------------------|------------------------|-------------------------|--------------------------|--------------------------|--------------------------|----------------|-------------------------|
| 1   | 0.50           | -1.50 | 2.500E+03<br>8.360E-05 | 0.000E-01<br>0.000E-01 | 1.943E-01<br>-2.510E-05 | -1.607E-01<br>-1.398E-08 | 2.500E+03<br>8.360E-05   | 1.948E-01<br>-2.510E-05  | -0.04<br>-0.04 | 2.500E+03<br>-1.599E-01 |
| 2   | 0.50           | -0.50 | 2.501E+03<br>8.360E-05 | 0.000E-01<br>0.000E-01 | 6.345E-01<br>-2.509E-05 | -1.451E-01<br>-1.262E-08 | 2.501E+03<br>8.360E-05   | 6.355E-01<br>-2.509E-05  | -0.03<br>-0.03 | 2.501E+03<br>-1.443E-01 |
| 3   | 0.50           | 0.50  | 2.501E+03<br>8.360E-05 | 0.000E-01<br>0.000E-01 | 6.650E-01<br>-2.509E-05 | 1.739E-01<br>1.512E-08   | 2.501E+03<br>8.360E-05   | 6.655E-01<br>-2.509E-05  | 0.04<br>0.04   | 2.501E+03<br>1.747E-01  |
| 4   | 0.50           | 1.50  | 2.500E+03<br>8.360E-05 | 0.000E-01<br>0.000E-01 | 1.978E-01<br>-2.510E-05 | 1.713E-01<br>1.489E-08   | 2.500E+03<br>8.360E-05   | 1.987E-01<br>-2.510E-05  | 0.04<br>0.04   | 2.500E+03<br>1.721E-01  |
| 5   | 1.50           | -1.50 | 2.501E+03<br>8.362E-05 | 0.000E-01<br>0.000E-01 | 5.308E-01<br>-2.510E-05 | -8.478E-01<br>-7.372E-08 | 2.501E+03<br>8.362E-05   | 5.317E-01<br>-2.510E-05  | -0.19<br>-0.19 | 2.501E+03<br>-8.470E-01 |
| 6   | 1.50           | -0.50 | 2.500E+03<br>8.357E-05 | 0.000E-01<br>0.000E-01 | 1.670E+00<br>-2.505E-05 | -7.189E-01<br>-6.251E-08 | 2.500E+03<br>8.357E-05   | 1.671E+00<br>-2.505E-05  | -0.16<br>-0.16 | 2.500E+03<br>-7.181E-01 |
| 7   | 1.50           | 0.50  | 2.500E+03<br>8.357E-05 | 0.000E-01<br>0.000E-01 | 1.665E+00<br>-2.505E-05 | 7.413E-01<br>6.446E-08   | 2.500E+03<br>8.357E-05   | 1.666E+00<br>-2.505E-05  | 0.17<br>0.17   | 2.500E+03<br>7.422E-01  |
| 8   | 1.50           | 1.50  | 2.501E+03<br>8.362E-05 | 0.000E-01<br>0.000E-01 | 5.261E-01<br>-2.510E-05 | 8.623E-01<br>7.499E-08   | 2.501E+03<br>8.362E-05   | 5.266E-01<br>-2.510E-05  | 0.20<br>0.20   | 2.501E+03<br>8.632E-01  |
| 9   | 2.50           | -1.50 | 2.503E+03<br>8.368E-05 | 0.000E-01<br>0.000E-01 | 1.117E+00<br>-2.510E-05 | -2.615E+00<br>-2.274E-07 | 2.503E+03<br>8.368E-05   | 1.116E+00<br>-2.510E-05  | -0.60<br>-0.60 | 2.503E+03<br>-2.614E+00 |
| 10  | 2.50           | -0.50 | 2.498E+03<br>8.349E-05 | 0.000E-01<br>0.000E-01 | 3.339E+00<br>-2.498E-05 | -1.952E+00<br>-1.698E-07 | 2.498E+03<br>8.349E-05   | 3.338E+00<br>-2.498E-05  | -0.45<br>-0.45 | 2.498E+03<br>-1.951E+00 |
| 11  | 2.50           | 0.50  | 2.498E+03<br>8.349E-05 | 0.000E-01<br>0.000E-01 | 3.334E+00<br>-2.498E-05 | 1.979E+00<br>1.721E-07   | 2.498E+03<br>8.349E-05   | 3.334E+00<br>-2.498E-05  | 0.45<br>0.45   | 2.498E+03<br>1.980E+00  |
| 12  | 2.50           | 1.50  | 2.503E+03<br>8.368E-05 | 0.000E-01<br>0.000E-01 | 1.112E+00<br>-2.510E-05 | 2.623E+00<br>2.281E-07   | 2.503E+03<br>8.368E-05   | 1.110E+00<br>-2.510E-05  | 0.60<br>0.60   | 2.503E+03<br>2.624E+00  |
| 13  | 3.50           | -1.50 | 2.507E+03<br>8.382E-05 | 0.000E-01<br>0.000E-01 | 9.927E-01<br>-2.514E-05 | -5.427E+00<br>-4.720E-07 | 2.507E+03<br>8.382E-05   | 9.814E-01<br>-2.515E-05  | -1.24<br>-1.24 | 2.507E+03<br>-5.427E+00 |
| 14  | 3.50           | -0.50 | 2.494E+03<br>8.336E-05 | 0.000E-01<br>0.000E-01 | 2.355E+00<br>-2.497E-05 | -3.358E+00<br>-2.920E-07 | 2.494E+03<br>8.336E-05   | 2.351E+00<br>-2.497E-05  | -0.77<br>-0.77 | 2.494E+03<br>-3.357E+00 |
| 15  | 3.50           | 0.50  | 2.494E+03<br>8.336E-05 | 0.000E-01<br>0.000E-01 | 2.353E+00<br>-2.497E-05 | 3.389E+00<br>2.947E-07   | 2.494E+03<br>8.336E-05   | 2.349E+00<br>-2.497E-05  | 0.78<br>0.78   | 2.494E+03<br>3.389E+00  |
| 16  | 3.50           | 1.50  | 2.507E+03<br>8.382E-05 | 0.000E-01<br>0.000E-01 | 9.929E-01<br>-2.514E-05 | 5.431E+00<br>4.723E-07   | 2.507E+03<br>8.382E-05   | 9.822E-01<br>-2.515E-05  | 1.24<br>1.24   | 2.507E+03<br>5.432E+00  |

- PAGE 7 -

| ELM | X1<br>MATERIAL | X3    | 1-STRESS<br>1-STRAIN   | 2-STRESS<br>2-STRAIN   | 3-STRESS<br>3-STRAIN     | 13-STRESS<br>13-STRAIN   | MAX-STRESS<br>MAX-STRAIN | MIN-STRESS<br>MIN-STRAIN | ANGLE            | JK-STRESS<br>JK-SHEAR   |
|-----|----------------|-------|------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|------------------|-------------------------|
| 17  | 4.50           | -1.50 | 2.512E+03<br>8.404E-05 | 0.000E-01<br>0.000E-01 | -3.942E+00<br>-2.536E-05 | -4.649E+00<br>-4.043E-07 | 2.512E+03<br>8.404E-05   | -3.949E+00<br>-2.536E-05 | -1.06<br>-1.06   | 2.512E+03<br>-4.648E+00 |
| 18  | 4.50           | -0.50 | 2.489E+03<br>8.336E-05 | 0.000E-01<br>0.000E-01 | -1.459E+01<br>-2.548E-05 | -3.114E-01<br>-2.708E-08 | 2.489E+03<br>8.336E-05   | -1.459E+01<br>-2.548E-05 | -0.07<br>-0.07   | 2.489E+03<br>-3.106E-01 |
| 19  | 4.50           | 0.50  | 2.489E+03<br>8.336E-05 | 0.000E-01<br>0.000E-01 | -1.458E+01<br>-2.548E-05 | 3.333E-01<br>2.898E-08   | 2.489E+03<br>8.336E-05   | -1.458E+01<br>-2.548E-05 | 0.08<br>0.03     | 2.489E+03<br>3.341E-01  |
| 20  | 4.50           | 1.50  | 2.512E+03<br>8.404E-05 | 0.000E-01<br>0.000E-01 | -3.941E+00<br>-2.536E-05 | 4.654E+00<br>4.047E-07   | 2.512E+03<br>8.404E-05   | -3.949E+00<br>-2.536E-05 | 1.06<br>1.06     | 2.512E+03<br>4.655E+00  |
| 21  | 5.50           | -1.50 | 2.502E+03<br>8.392E-05 | 0.000E-01<br>0.000E-01 | -2.501E+01<br>-2.597E-05 | 1.981E+01<br>1.723E-06   | 2.502E+03<br>8.393E-05   | -2.517E+01<br>-2.597E-05 | 4.49<br>4.49     | 2.502E+03<br>1.981E+01  |
| 22  | 5.50           | -0.50 | 2.498E+03<br>8.436E-05 | 0.000E-01<br>0.000E-01 | -8.227E+01<br>-2.784E-05 | 2.381E+01<br>2.071E-06   | 2.499E+03<br>8.437E-05   | -8.249E+01<br>-2.785E-05 | 5.29<br>5.29     | 2.498E+03<br>2.381E+01  |
| 23  | 5.50           | 0.50  | 2.498E+03<br>8.437E-05 | 0.000E-01<br>0.000E-01 | -8.227E+01<br>-2.784E-05 | -2.380E+01<br>-2.070E-06 | 2.499E+03<br>8.437E-05   | -8.249E+01<br>-2.785E-05 | -5.28<br>-5.28   | 2.498E+03<br>-2.380E+01 |
| 24  | 5.50           | 1.50  | 2.502E+03<br>8.392E-05 | 0.000E-01<br>0.000E-01 | -2.501E+01<br>-2.597E-05 | -1.980E+01<br>-1.722E-06 | 2.503E+03<br>8.393E-05   | -2.516E+01<br>-2.597E-05 | -4.49<br>-4.49   | 2.502E+03<br>-1.980E+01 |
| 25  | 6.50           | -1.50 | 2.421E+03<br>8.174E-05 | 0.000E-01<br>0.000E-01 | -7.836E+01<br>-2.693E-05 | 1.215E+02<br>1.057E-05   | 2.427E+03<br>8.199E-05   | -8.425E+01<br>-2.719E-05 | 27.77<br>27.77   | 2.421E+03<br>1.215E+02  |
| 26  | 6.50           | -0.50 | 2.580E+03<br>8.884E-05 | 0.000E-01<br>0.000E-01 | -2.574E+02<br>-3.451E-05 | 1.105E+02<br>9.609E-06   | 2.584E+03<br>8.902E-05   | -2.617E+02<br>-3.470E-05 | 22.27<br>22.27   | 2.580E+03<br>1.105E+02  |
| 27  | 6.50           | 0.50  | 2.580E+03<br>8.884E-05 | 0.000E-01<br>0.000E-01 | -2.574E+02<br>-3.451E-05 | -1.105E+02<br>-9.609E-06 | 2.584E+03<br>8.902E-05   | -2.617E+02<br>-3.470E-05 | -22.27<br>-22.27 | 2.580E+03<br>-1.105E+02 |
| 28  | 6.50           | 1.50  | 2.421E+03<br>8.174E-05 | 0.000E-01<br>0.000E-01 | -7.837E+01<br>-2.693E-05 | -1.215E+02<br>-1.056E-05 | 2.427E+03<br>8.199E-05   | -8.426E+01<br>-2.719E-05 | -27.76<br>-27.76 | 2.421E+03<br>-1.215E+02 |
| 29  | 7.50           | -1.50 | 2.130E+03<br>7.300E-05 | 0.000E-01<br>0.000E-01 | -1.756E+02<br>-2.727E-05 | 3.880E+02<br>3.374E-05   | 2.194E+03<br>7.576E-05   | -2.391E+02<br>-3.003E-05 | 92.99<br>92.99   | 2.130E+03<br>3.880E+02  |
| 30  | 7.50           | -0.50 | 2.870E+03<br>1.012E-04 | 0.000E-01<br>0.000E-01 | -5.258E+02<br>-4.640E-05 | 3.215E+02<br>2.796E-05   | 2.900E+03<br>1.026E-04   | -5.559E+02<br>-4.771E-05 | 53.62<br>53.62   | 2.870E+03<br>3.215E+02  |
| 31  | 7.50           | 0.50  | 2.870E+03<br>1.012E-04 | 0.000E-01<br>0.000E-01 | -5.258E+02<br>-4.640E-05 | -3.215E+02<br>-2.796E-05 | 2.900E+03<br>1.026E-04   | -5.559E+02<br>-4.771E-05 | -53.62<br>-53.62 | 2.870E+03<br>-3.215E+02 |
| 32  | 7.50           | 1.50  | 2.130E+03<br>7.300E-05 | 0.000E-01<br>0.000E-01 | -1.756E+02<br>-2.727E-05 | -3.880E+02<br>-3.374E-05 | 2.194E+03<br>7.576E-05   | -2.391E+02<br>-3.003E-05 | -92.99<br>-92.99 | 2.130E+03<br>-3.880E+02 |

- PAGE 8 -

| ELM | X1<br>MATERIAL | X3    | 1-STRESS<br>1-STRAIN    | 2-STRESS<br>2-STRAIN   | 3-STRESS<br>3-STRAIN     | 13-STRESS<br>13-STRAIN   | MAX-STRESS<br>MAX-STRAIN | MIN-STRESS<br>MIN-STRAIN | ANGLE            | JK-STRESS<br>JK-SHEAR   |
|-----|----------------|-------|-------------------------|------------------------|--------------------------|--------------------------|--------------------------|--------------------------|------------------|-------------------------|
| 33  | 8.50           | -1.50 | 1.419E+03<br>4.584E-05  | 0.000E-01<br>0.000E-01 | 1.609E+02<br>-8.872E-06  | 7.091E+02<br>6.166E-05   | 1.738E+03<br>5.970E-05   | -1.579E+02<br>-2.273E-05 | 242.09<br>242.09 | 1.419E+03<br>7.091E+02  |
| 34  | 8.50           | -0.50 | 3.581E+03<br>1.258E-04  | 0.000E-01<br>0.000E-01 | -6.038E+02<br>-5.615E-05 | 8.845E+02<br>7.692E-05   | 3.760E+03<br>1.336E-04   | -7.830E+02<br>-6.394E-05 | 114.58<br>114.58 | 3.581E+03<br>8.845E+02  |
| 35  | 8.50           | 0.50  | 3.581E+03<br>1.258E-04  | 0.000E-01<br>0.000E-01 | -6.038E+02<br>-5.615E-05 | -8.845E+02<br>-7.691E-05 | 3.760E+03<br>1.336E-04   | -7.830E+02<br>-6.394E-05 | 114.58<br>114.58 | 3.581E+03<br>-8.845E+02 |
| 36  | 8.50           | 1.50  | 1.419E+03<br>4.584E-05  | 0.000E-01<br>0.000E-01 | 1.609E+02<br>-8.872E-06  | -7.091E+02<br>-6.166E-05 | 1.738E+03<br>5.970E-05   | -1.579E+02<br>-2.273E-05 | 242.09<br>242.09 | 1.419E+03<br>-7.091E+02 |
| 37  | 9.50           | -1.50 | 1.839E+01<br>-5.814E-07 | 0.000E-01<br>0.000E-01 | 1.191E+02<br>3.798E-06   | 2.503E+01<br>2.178E-06   | 1.250E+02<br>4.053E-06   | 1.251E+01<br>-8.369E-07  | 767.87<br>767.87 | 1.839E+01<br>2.503E+01  |
| 38  | 9.50           | -0.50 | 4.982E+03<br>1.517E-04  | 0.000E-01<br>0.000E-01 | 1.476E+03<br>-6.823E-07  | 2.416E+03<br>2.101E-04   | 6.214E+03<br>2.053E-04   | 2.438E+02<br>-5.425E-05  | 270.19<br>270.19 | 4.982E+03<br>2.416E+03  |
| 39  | 9.50           | 0.50  | 4.982E+03<br>1.517E-04  | 0.000E-01<br>0.000E-01 | 1.476E+03<br>-6.823E-07  | -2.416E+03<br>-2.101E-04 | 6.214E+03<br>2.053E-04   | 2.438E+02<br>-5.425E-05  | 270.19<br>270.19 | 4.982E+03<br>-2.416E+03 |
| 40  | 9.50           | 1.50  | 1.839E+01<br>-5.814E-07 | 0.000E-01<br>0.000E-01 | 1.191E+02<br>3.798E-06   | -2.503E+01<br>-2.178E-06 | 1.250E+02<br>4.053E-06   | 1.251E+01<br>-8.368E-07  | 767.88<br>767.88 | 1.839E+01<br>-2.503E+01 |

COMPUTATIONS COMPLETED

Additional test problems were run to checkout other functions and options of the computer code. Results of these tests are summarized briefly below. For each problem the input data is listed for reference purposes. All test problems use the same grid system as problem # 7, with only loading or constraint conditions changed.

#### LOPE Test Problem #8

In this test the concentrated force was replaced by a compressive pressure loading along the unsupported bottom edge of the rod. Thus, the rod is loaded uniformly and the stress in all elements should be  $\sigma_x = 2500$  psi, with all other components zero. This result was obtained from the computer solution, but is not listed; however the input data for this problem is listed in Table 4. The nodal displacements were also constant across the rod and became progressively larger with distance X along the rod. The displacement state is shown by the dashed line grid in Figure 6. The theoretically computed displacement of the loaded end of the rod is

$$\delta = - \frac{PL}{AE} = - \frac{2500(4 \times 10)}{4(30 \times 10^6)} = -8.3333 \times 10^{-4} \text{ in.}$$

which compares well with the computer predicted value  $\delta = -8.3604 \times 10^{-4}$  in.

A second version of the uniformly loaded rod was run to checkout the gridpoint constraint function of the program. The uniform pressure was applied as before, but gridpoint #51 was constrained to move at a 45° angle to the axis of loading. This caused the distortion in displacement of the rod, as noted in Figure 7. No quantitative analytical results are known for this test case, only that the displacement state conforms to the constraint condition that was imposed. The input data for this problem is listed in Table 5.

#### LOPE Test Problem #9

This problem tests the application of a shear boundary stress, similar to



TABLE 4 : COMPUTER INPUT DATA FOR TEST PROBLEM #8

| LOPE TEST PROBLEM #8 |      |     |      |     |      |      |      |     |      |     |
|----------------------|------|-----|------|-----|------|------|------|-----|------|-----|
| 1                    |      |     |      |     |      |      |      |     |      |     |
| 2                    | 55   | 40  | 1    | 4   | 2    | 0.0  | 0.0  |     |      |     |
| 3                    | 1    |     | 0.0  |     |      |      |      |     |      |     |
| 4                    | .403 | E08 | .173 | E08 | .173 | E08  | .403 | E08 | .173 | E08 |
| 5                    | 1    | 1   | 0.0  |     |      | -2.0 | 0.0  |     |      |     |
| 6                    | 2    | 1   | 0.0  |     |      | -1.0 | 0.0  |     |      |     |
| 7                    | 3    | 11  | 0.0  |     |      | 0.0  | 0.0  | 0.0 |      |     |
| 8                    | 4    | 1   | 0.0  |     |      | 1.0  | 0.0  |     |      |     |
| 9                    | 5    | 1   | 0.0  |     |      | 2.0  | 0.0  |     |      |     |
| 10                   | 6    |     | 1.0  |     |      | -2.0 |      |     |      |     |
| 11                   | 10   |     | 1.0  |     |      | 2.0  |      |     |      |     |
| 12                   | 11   |     | 2.0  |     |      | -2.0 |      |     |      |     |
| 13                   | 15   |     | 2.0  |     |      | 2.0  |      |     |      |     |
| 14                   | 16   |     | 3.0  |     |      | -2.0 |      |     |      |     |
| 15                   | 20   |     | 3.0  |     |      | 2.0  |      |     |      |     |
| 16                   | 21   |     | 4.0  |     |      | -2.0 |      |     |      |     |
| 17                   | 25   |     | 4.0  |     |      | 2.0  |      |     |      |     |
| 18                   | 26   |     | 5.0  |     |      | -2.0 |      |     |      |     |
| 19                   | 30   |     | 5.0  |     |      | 2.0  |      |     |      |     |
| 20                   | 31   |     | 6.0  |     |      | -2.0 |      |     |      |     |
| 21                   | 35   |     | 6.0  |     |      | 2.0  |      |     |      |     |
| 22                   | 36   |     | 7.0  |     |      | -2.0 |      |     |      |     |
| 23                   | 40   |     | 7.0  |     |      | 2.0  |      |     |      |     |
| 24                   | 41   |     | 8.0  |     |      | -2.0 |      |     |      |     |
| 25                   | 45   |     | 8.0  |     |      | 2.0  |      |     |      |     |
| 26                   | 46   |     | 9.0  |     |      | -2.0 |      |     |      |     |
| 27                   | 50   |     | 9.0  |     |      | 2.0  |      |     |      |     |
| 28                   | 51   |     | 10.0 |     |      | -2.0 |      |     |      |     |
| 29                   | 52   |     | 10.0 |     |      | -1.0 |      |     |      |     |
| 30                   | 53   |     | 10.0 |     |      | 0.0  |      |     |      |     |
| 31                   | 54   |     | 10.0 |     |      | 1.0  |      |     |      |     |
| 32                   | 55   |     | 10.0 |     |      | 2.0  |      |     |      |     |
| 33                   | 1    | 1   | 6    | 7   | 2    | 1    |      |     |      |     |
| 34                   | 5    | 6   | 11   | 12  | 7    | 1    |      |     |      |     |
| 35                   | 9    | 11  | 16   | 17  | 12   | 1    |      |     |      |     |
| 36                   | 13   | 16  | 21   | 22  | 17   | 1    |      |     |      |     |
| 37                   | 17   | 21  | 26   | 27  | 22   | 1    |      |     |      |     |
| 38                   | 21   | 26  | 31   | 32  | 27   | 1    |      |     |      |     |
| 39                   | 25   | 31  | 36   | 37  | 32   | 1    |      |     |      |     |
| 40                   | 29   | 36  | 41   | 42  | 37   | 1    |      |     |      |     |
| 41                   | 33   | 41  | 46   | 47  | 42   | 1    |      |     |      |     |
| 42                   | 37   | 46  | 51   | 52  | 47   | 1    |      |     |      |     |
| 43                   | 40   | 49  | 54   | 55  | 50   | 1    |      |     |      |     |
| 44                   | 51   | 52  |      |     |      | 2500 |      |     |      |     |
| 45                   | 52   | 53  |      |     |      | 2500 |      |     |      |     |
| 46                   | 53   | 54  |      |     |      | 2500 |      |     |      |     |
| 47                   | 54   | 55  |      |     |      | 2500 |      |     |      |     |

Figure 6 : DISPLACEMENT STATE OF UNIFORMLY LOADED ROD

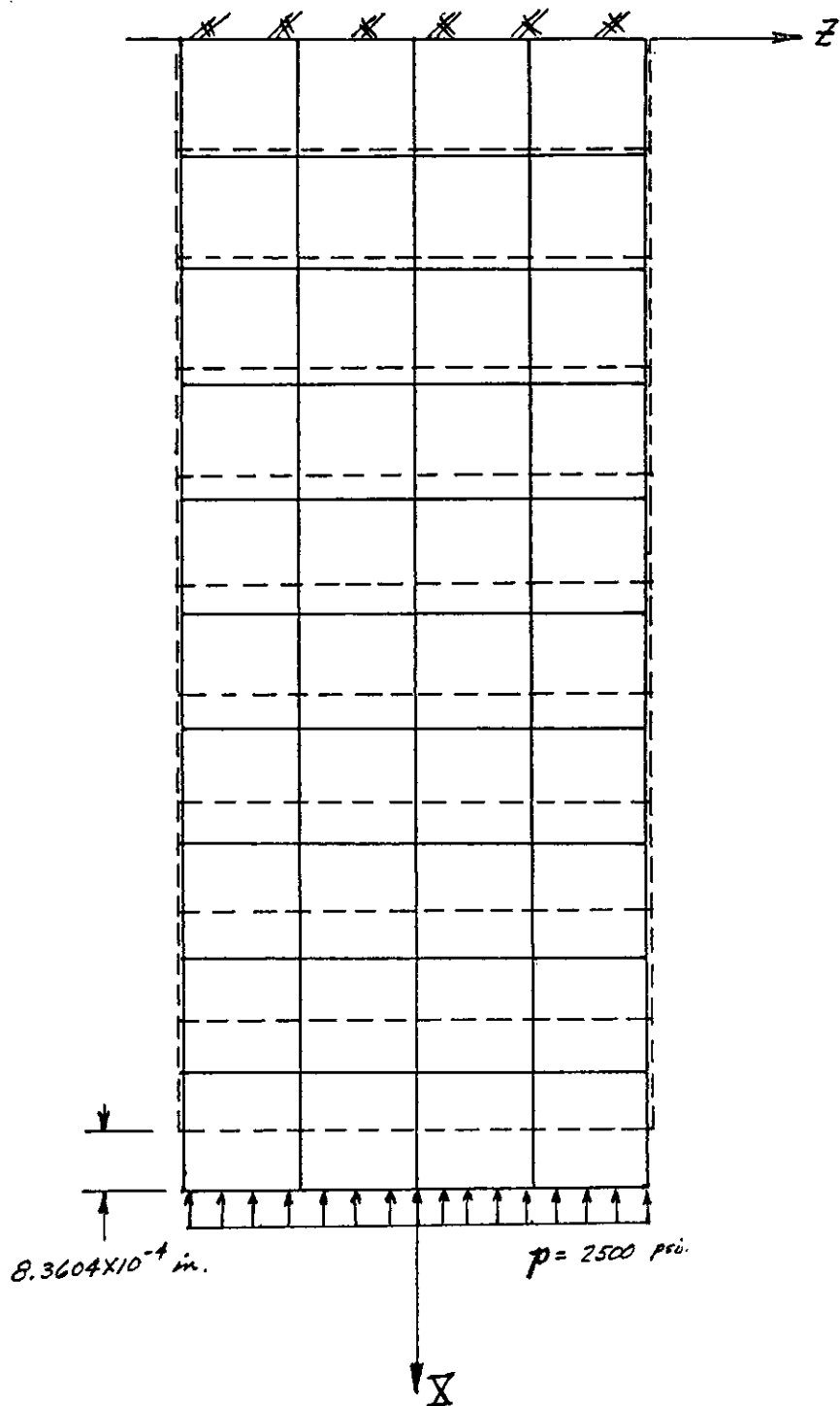


Figure 7 : UNIFORMLY LOADED ROD WITH DISPLACEMENT  
CONSTRAINT CONDITION

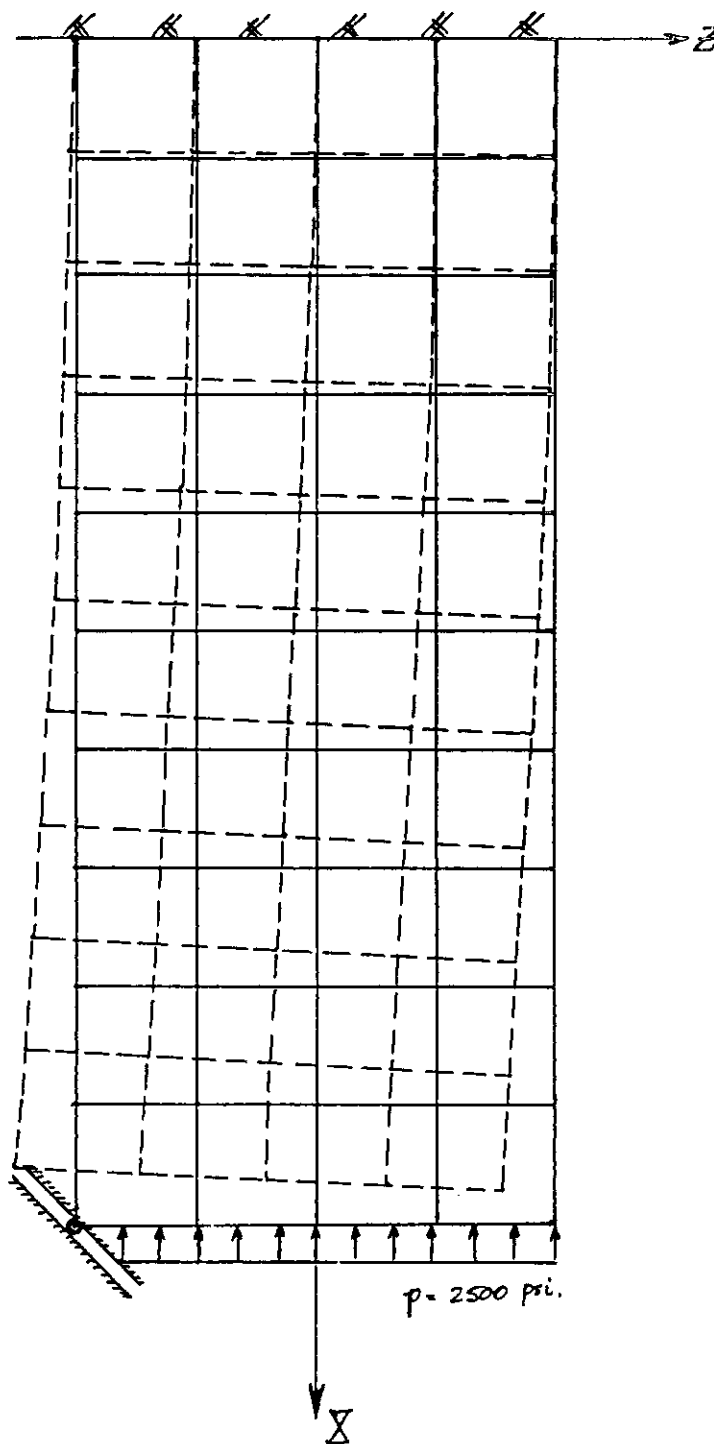


TABLE 5 : LISTING OF INPUT DATA FOR TEST PROBLEM  
#8, WITH A CONSTRAINED NODAL POINT

| LOPE TEST PROBLEM #8 - WITH CONSTRAINED NODE |      |     |      |            |      |     |      |     |      |     |
|----------------------------------------------|------|-----|------|------------|------|-----|------|-----|------|-----|
| 1                                            | 55   | 40  | 1    | 4          | 2    | 0.0 | 0.0  |     |      |     |
| 2                                            | 1    |     | 0.0  | MILD STEEL |      |     |      |     |      |     |
| 3                                            | .403 | E08 | .173 | E08        | .173 | E08 | .403 | E08 | .173 | E08 |
| 4                                            | .403 | E08 | .173 | E08        | .173 | E08 | .403 | E08 | .173 | E08 |
| 5                                            | 1    | 1   | 0.0  | -2.0       | 0.0  |     |      |     |      |     |
| 6                                            | 2    | 1   | 0.0  | -1.0       | 0.0  |     |      |     |      |     |
| 7                                            | 3    | 11  | 0.0  | 0.0        | 0.0  |     |      | 0.0 |      |     |
| 8                                            | 4    | 1   | 0.0  | 1.0        | 0.0  |     |      |     |      |     |
| 9                                            | 5    | 1   | 0.0  | 2.0        | 0.0  |     |      |     |      |     |
| 10                                           | 6    |     | 1.0  | -2.0       |      |     |      |     |      |     |
| 11                                           | 10   |     | 1.0  | 2.0        |      |     |      |     |      |     |
| 12                                           | 11   |     | 2.0  | -2.0       |      |     |      |     |      |     |
| 13                                           | 15   |     | 2.0  | 2.0        |      |     |      |     |      |     |
| 14                                           | 16   |     | 3.0  | -2.0       |      |     |      |     |      |     |
| 15                                           | 20   |     | 3.0  | 2.0        |      |     |      |     |      |     |
| 16                                           | 21   |     | 4.0  | -2.0       |      |     |      |     |      |     |
| 17                                           | 25   |     | 4.0  | 2.0        |      |     |      |     |      |     |
| 18                                           | 26   |     | 5.0  | -2.0       |      |     |      |     |      |     |
| 19                                           | 30   |     | 5.0  | 2.0        |      |     |      |     |      |     |
| 20                                           | 31   |     | 6.0  | -2.0       |      |     |      |     |      |     |
| 21                                           | 35   |     | 6.0  | 2.0        |      |     |      |     |      |     |
| 22                                           | 36   |     | 7.0  | -2.0       |      |     |      |     |      |     |
| 23                                           | 40   |     | 7.0  | 2.0        |      |     |      |     |      |     |
| 24                                           | 41   |     | 8.0  | -2.0       |      |     |      |     |      |     |
| 25                                           | 45   |     | 8.0  | 2.0        |      |     |      |     |      |     |
| 26                                           | 46   |     | 9.0  | -2.0       |      |     |      |     |      |     |
| 27                                           | 50   |     | 9.0  | 2.0        |      |     |      |     |      |     |
| 28                                           | 51   |     | 10.0 | -2.0       |      |     |      |     | 45   |     |
| 29                                           | 52   |     | 10.0 | -1.0       |      |     |      |     |      |     |
| 30                                           | 53   |     | 10.0 | 0.0        |      |     |      |     |      |     |
| 31                                           | 54   |     | 10.0 | 1.0        |      |     |      |     |      |     |
| 32                                           | 55   |     | 10.0 | 2.0        |      |     |      |     |      |     |
| 33                                           | 1    | 1   | 6    | 7          | 2    | 1   |      |     |      |     |
| 34                                           | 5    | 6   | 11   | 12         | 7    | 1   |      |     |      |     |
| 35                                           | 9    | 11  | 16   | 17         | 12   | 1   |      |     |      |     |
| 36                                           | 13   | 16  | 21   | 22         | 17   | 1   |      |     |      |     |
| 37                                           | 17   | 21  | 26   | 27         | 22   | 1   |      |     |      |     |
| 38                                           | 21   | 26  | 31   | 32         | 27   | 1   |      |     |      |     |
| 39                                           | 25   | 31  | 36   | 37         | 32   | 1   |      |     |      |     |
| 40                                           | 29   | 36  | 41   | 42         | 37   | 1   |      |     |      |     |
| 41                                           | 33   | 41  | 46   | 47         | 42   | 1   |      |     |      |     |
| 42                                           | 37   | 46  | 51   | 52         | 47   | 1   |      |     |      |     |
| 43                                           | 40   | 49  | 54   | 55         | 50   | 1   |      |     |      |     |
| 44                                           | 51   | 52  | 2500 |            |      |     |      |     |      |     |
| 45                                           | 52   | 53  | 2500 |            |      |     |      |     |      |     |
| 46                                           | 53   | 54  | 2500 |            |      |     |      |     |      |     |
| 47                                           | 54   | 55  | 2500 |            |      |     |      |     |      |     |

the normal boundary pressure of problem #8. The grid layout, loading, and displacement state are shown in Figure 8. The problem is basically a cantilever beam subjected to a 10,000LB force at its free end. For this configuration the theoretical analytical maximum deflection at the end of the beam is

$$\delta = \frac{PL^3}{3EI} = \frac{10,000 (10)^3}{3(30 \times 10^6) \left(\frac{1 \times 4}{12}\right)^3} = 2.08 \times 10^{-2} \text{ in.}$$

compared to the computer determined value of  $S = 2.2743 \times 10^{-2}$  in., an error of 9.3%. Part of this error is likely due to the type of cantilever support condition assumed, in which the beam is free to expand in the Z direction except at the centerline gridpoint (#3). Input data for this problem is listed in Table 6.

#### LOPE Test Problem #10

This test problem involved the evaluation of the axial rod of test problem #7 under gravitational loading along the X axis. For this calculation acceleration along the X axis was input as  $ACEL1 = 384.4 \text{ in/sec}^2$ , and density of the material was set at  $\rho = 0.001 \text{ lb-sec}^2/\text{in}^4$ .

Only the input data listing is given for this problem (Table 7). The results obtained by the computer calculation, agree well with the exact solution to the problem. The axial stress computed at the centroid of the finite elements next to the upper support was  $\sigma_x = 3.62 \text{ psi}$ , compared to the exact value of  $\sigma_x = 3.65 \text{ psi}$ . Displacement at the lower, free end of the rod by computer solution was  $\delta = 6.380 \times 10^{-7} \text{ in.}$ , compared to the exact solution of  $\delta = 6.40 \times 10^{-7} \text{ in.}$

#### References

Goudreau, G.L., Nickeu, R.E., Dunham, R.S., 1967. 'Plane and axisymmetric finite element analysis of locally orthotropic elastic solids and orthotropic shells', University of California, Berkeley, California, Report 67-15.

Figure 8 : LOADING AND DISPLACEMENT STATE TEST  
PROBLEM #9

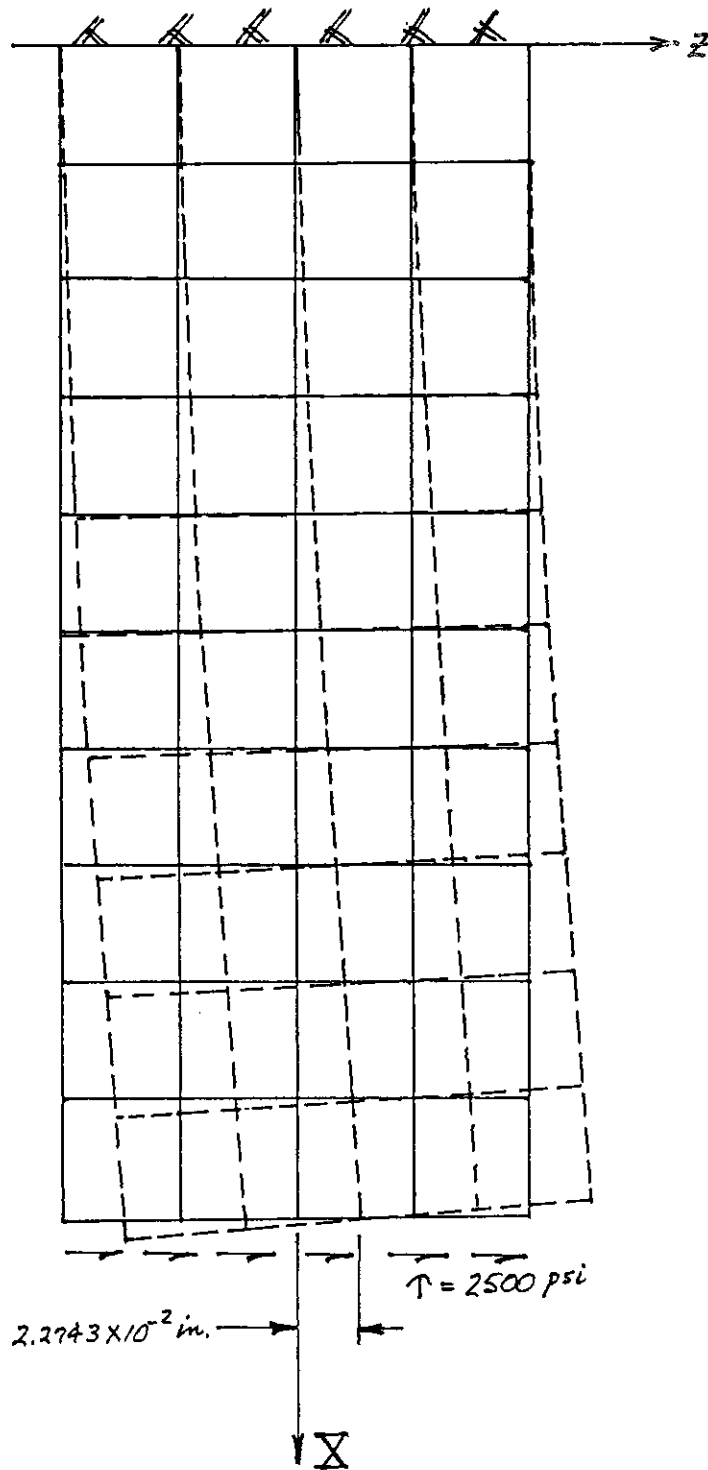


TABLE 6 : INPUT DATA FOR TEST PROBLEM #9

| LOPE TEST PROBLEM #9 |      |     |      |            |      |      |      |     |      |     |
|----------------------|------|-----|------|------------|------|------|------|-----|------|-----|
| 1                    | 55   | 40  | 1    | 4          | 2    | 0.0  | 0.0  |     |      |     |
| 2                    | 1    |     | 0.0  | MILD STEEL |      |      |      |     |      |     |
| 3                    | .403 | E08 | .173 | E08        | .173 | E08  | .403 | E08 | .173 | E08 |
| 4                    | 1    | 1   |      | 0.0        | -2.0 |      | 0.0  |     |      |     |
| 5                    | 2    | 1   |      | 0.0        | -1.0 |      | 0.0  |     |      |     |
| 6                    | 3    | 11  |      | 0.0        | 0.0  |      | 0.0  | 0.0 |      |     |
| 7                    | 4    | 1   |      | 0.0        | 1.0  |      | 0.0  |     |      |     |
| 8                    | 5    | 1   |      | 0.0        | 2.0  |      | 0.0  |     |      |     |
| 9                    | 6    |     |      | 1.0        | -2.0 |      |      |     |      |     |
| 10                   | 10   |     |      | 1.0        | 2.0  |      |      |     |      |     |
| 11                   | 11   |     |      | 2.0        | -2.0 |      |      |     |      |     |
| 12                   | 15   |     |      | 2.0        | 2.0  |      |      |     |      |     |
| 13                   | 16   |     |      | 3.0        | -2.0 |      |      |     |      |     |
| 14                   | 20   |     |      | 3.0        | 2.0  |      |      |     |      |     |
| 15                   | 21   |     |      | 4.0        | -2.0 |      |      |     |      |     |
| 16                   | 25   |     |      | 4.0        | 2.0  |      |      |     |      |     |
| 17                   | 26   |     |      | 5.0        | -2.0 |      |      |     |      |     |
| 18                   | 30   |     |      | 5.0        | 2.0  |      |      |     |      |     |
| 19                   | 31   |     |      | 6.0        | -2.0 |      |      |     |      |     |
| 20                   | 35   |     |      | 6.0        | 2.0  |      |      |     |      |     |
| 21                   | 36   |     |      | 7.0        | -2.0 |      |      |     |      |     |
| 22                   | 40   |     |      | 7.0        | 2.0  |      |      |     |      |     |
| 23                   | 41   |     |      | 8.0        | -2.0 |      |      |     |      |     |
| 24                   | 45   |     |      | 8.0        | 2.0  |      |      |     |      |     |
| 25                   | 46   |     |      | 9.0        | -2.0 |      |      |     |      |     |
| 26                   | 50   |     |      | 9.0        | 2.0  |      |      |     |      |     |
| 27                   | 51   |     |      | 10.0       | -2.0 |      |      |     |      |     |
| 28                   | 52   |     |      | 10.0       | -1.0 |      |      |     |      |     |
| 29                   | 53   |     |      | 10.0       | 0.0  |      |      |     |      |     |
| 30                   | 54   |     |      | 10.0       | 1.0  |      |      |     |      |     |
| 31                   | 55   |     |      | 10.0       | 2.0  |      |      |     |      |     |
| 32                   | 1    | 1   | 6    | 7          | 2    | 1    |      |     |      |     |
| 33                   | 5    | 6   | 11   | 12         | 7    | 1    |      |     |      |     |
| 34                   | 9    | 11  | 16   | 17         | 12   | 1    |      |     |      |     |
| 35                   | 13   | 16  | 21   | 22         | 17   | 1    |      |     |      |     |
| 36                   | 17   | 21  | 26   | 27         | 22   | 1    |      |     |      |     |
| 37                   | 21   | 26  | 31   | 32         | 27   | 1    |      |     |      |     |
| 38                   | 25   | 31  | 36   | 37         | 32   | 1    |      |     |      |     |
| 39                   | 29   | 36  | 41   | 42         | 37   | 1    |      |     |      |     |
| 40                   | 33   | 41  | 46   | 47         | 42   | 1    |      |     |      |     |
| 41                   | 37   | 46  | 51   | 52         | 47   | 1    |      |     |      |     |
| 42                   | 40   | 49  | 54   | 55         | 50   | 1    |      |     |      |     |
| 43                   | 51   | 52  |      |            |      | 2500 |      |     |      |     |
| 44                   | 52   | 53  |      |            |      | 2500 |      |     |      |     |
| 45                   | 53   | 54  |      |            |      | 2500 |      |     |      |     |
| 46                   | 54   | 55  |      |            |      | 2500 |      |     |      |     |

TABLE 7 : INPUT DATA FOR TEST PROBLEM #10

| 1  | LOPE TEST PROBLEM #10 |          |    |      |      |   |
|----|-----------------------|----------|----|------|------|---|
| 2  | 55                    | 40       | 1  | 0    | 2    | 3 |
| 3  | 1                     | 0.001    |    |      |      |   |
| 4  | .403 E08              | .173 E08 |    |      |      |   |
| 5  | 1                     | 1        |    | 0.0  | -2.0 |   |
| 6  | 2                     | 1        |    | 0.0  | -1.0 |   |
| 7  | 3                     | 11       |    | 0.0  | 0.0  |   |
| 8  | 4                     | 1        |    | 0.0  | 1.0  |   |
| 9  | 5                     | 1        |    | 0.0  | 2.0  |   |
| 10 | 6                     |          |    | 1.0  | -2.0 |   |
| 11 | 10                    |          |    | 1.0  | 2.0  |   |
| 12 | 11                    |          |    | 2.0  | -2.0 |   |
| 13 | 15                    |          |    | 2.0  | 2.0  |   |
| 14 | 16                    |          |    | 3.0  | -2.0 |   |
| 15 | 20                    |          |    | 3.0  | 2.0  |   |
| 16 | 21                    |          |    | 4.0  | -2.0 |   |
| 17 | 25                    |          |    | 4.0  | 2.0  |   |
| 18 | 26                    |          |    | 5.0  | -2.0 |   |
| 19 | 30                    |          |    | 5.0  | 2.0  |   |
| 20 | 31                    |          |    | 6.0  | -2.0 |   |
| 21 | 35                    |          |    | 6.0  | 2.0  |   |
| 22 | 36                    |          |    | 7.0  | -2.0 |   |
| 23 | 40                    |          |    | 7.0  | 2.0  |   |
| 24 | 41                    |          |    | 8.0  | -2.0 |   |
| 25 | 45                    |          |    | 8.0  | 2.0  |   |
| 26 | 46                    |          |    | 9.0  | -2.0 |   |
| 27 | 50                    |          |    | 9.0  | 2.0  |   |
| 28 | 51                    |          |    | 10.0 | -2.0 |   |
| 29 | 52                    |          |    | 10.0 | -1.0 |   |
| 30 | 53                    |          |    | 10.0 | 0.0  |   |
| 31 | 54                    |          |    | 10.0 | 1.0  |   |
| 32 | 55                    |          |    | 10.0 | 2.0  |   |
| 33 | 1                     | 1        | 6  | 7    | 2    | 1 |
| 34 | 5                     | 6        | 11 | 12   | 7    | 1 |
| 35 | 9                     | 11       | 16 | 17   | 12   | 1 |
| 36 | 13                    | 16       | 21 | 22   | 17   | 1 |
| 37 | 17                    | 21       | 26 | 27   | 22   | 1 |
| 38 | 21                    | 26       | 31 | 32   | 27   | 1 |
| 39 | 25                    | 31       | 36 | 37   | 32   | 1 |
| 40 | 29                    | 36       | 41 | 42   | 37   | 1 |
| 41 | 33                    | 41       | 46 | 47   | 42   | 1 |
| 42 | 37                    | 46       | 51 | 52   | 47   | 1 |
| 43 | 40                    | 49       | 54 | 55   | 50   | 1 |



Timoshenko, S.P. and Goodier, J.N., 1970. Theory of elasticity, third edition, M Graw-Hill, N.Y., New York, p.59.

APPENDIX

MAIN PROGRAM AND SUBROUTINE LISTING

REAL TIME FORTRAN VER.E00 PAGE 1 DATE 83 08 23

```

1      C      * LOCAL ORTHOTROPIC PLANAR ELASTICITY PROGRAM
2          DIMENSION LM(4),EPS(8),SIG(8)
3          COMMON A(54,108),B(108)
4          COMMON/NPELD/E(7,10),RO(10),CODE(600),X(600),Y(600),
5          *UX(1200),IX(500,5),ANGLE(500),NUMNP,NUMEL,NUMPC
6          COMMON/QADTRI/XXX(5),YYY(5),C(4,4),S(10,10),P(10)
7          DATA PII/28.648/
8      C      * * * * * PARAMETER INITIALIZATION
9          NB=27
10         ISTOP=0
11         NUMBLK=0
12         IJK=0
13         NEL=0
14         CALL LOCATE(NPP,ISTOP,ACEL1,ACEL3,NB,MBAND)
15         IF(ISTOP.NE.0) GO TO 999
16      C      * * * * * OTHER INITIALIZATION
17         ND=2*NB
18         ND2=4*NB
19         DO 5 N=1,ND2
20             B(N)=0.0
21             DO 5 M=1,ND
22                 5 A(M,N)=0.0
23      C      * * * * * FORM STIFFNESS MATRIX IN BLOCKS
24         6 NUMBLK=NUMBLK+1
25         NM=NB*NUMBLK
26         NL=NM-NB+1
27         NT=NM+MBAND
28         NEL=NEL+1
29         KSHIFT=2*NL-2
30         IF(NM.GT.NUMNP) NM=NUMNP
31         IF(NEL.GE.NUMEL) GO TO 210
32      C      * * * * * SELECT ELEMENT IN BLOCK
33         DO 210 N=NEL,NUMEL
34             MT=IX(N,5)
35             IF(MT.GT.0) GO TO 10
36             WRITE(6,3001) N
37             GO TO 210
38         10 AM1=ACEL1*RO(MT)
39             AM3=ACEL3*RO(MT)
40             DO 7 I=1,4
41                 IF(IX(N,I).LT.NL) GO TO 7
42                 IF(IX(N,I).LE.NT) GO TO 8
43             7 CONTINUE
44             GO TO 210
45         8 IF(N.GT.NEL) NEL=N
46             DO 9 I=1,10
47                 P(I)=0.0
48             DO 9 J=1,10
49                 9 S(I,J)=0.0
50             IF(ISTOP.NE.0) GO TO 90
51      C      * * * * * FORM STRESS-STRAIN RELATIONSHIP
52             CALL MODULI(N,I,J,K,L)
53             DO 80 M=1,4
54                 C(M,2)=0.0

```

REAL TIME FORTRAN VER.E00 PAGE 2 DATE 83 08 23

```

55      80 C(2,M)=0.0
56      C      *      *      *      *      FORM QUADRILATERAL STIFFNESS MATRIX
57      90 DO 100 M=1,4
58          MM=IX(N,M)
59          XXX(M)=X(MM)
60      100 YYY(M)=Y(MM)
61          IF(K.NE.L) GO TO 110
62          CALL TRISTF(1,2,3,NPP,ISTOP,COMM,AM1,AM3)
63          IF(COMM.LE.0.0) GO TO 190
64          GO TO 120
65      110 XXX(5)=0.25*(XXX(1)+XXX(2)+XXX(3)+XXX(4))
66          YYY(5)=0.25*(YYY(1)+YYY(2)+YYY(3)+YYY(4))
67          CALL TRISTF(1,2,5,NPP,ISTOP,COMM,AM1,AM3)
68          IF(COMM.LE.0.0) GO TO 190
69          CALL TRISTF(2,3,5,NPP,ISTOP,COMM,AM1,AM3)
70          IF(COMM.LE.0.0) GO TO 190
71          CALL TRISTF(3,4,5,NPP,ISTOP,COMM,AM1,AM3)
72          IF(COMM.LE.0.0) GO TO 190
73          CALL TRISTF(4,1,5,NPP,ISTOP,COMM,AM1,AM3)
74          IF(COMM.LE.0.0) GO TO 190
75      120 IF(ISTOP.NE.0) GO TO 210
76      C      *      *      SOLVE FOR MIDDLE NODAL POINT DISPLACEMENTS
77          IF(K.EQ.L) GO TO 170
78          DO 150 I=1,9
79              CC=S(I,10)/S(10,10)
80              P(I)=P(I)-CC*P(10)
81          DO 150 J=1,9
82      150 S(I,J)=S(I,J)-CC*S(10,J)
83          DO 160 I=1,8
84              CC=S(I,9)/S(9,9)
85              P(I)=P(I)-CC*P(9)
86          DO 160 J=1,8
87      160 S(I,J)=S(I,J)-CC*S(9,J)
88      170 CONTINUE
89          GO TO 200
90      190 WRITE(6,3000) N
91          ISTOP=1
92          IF(ISTOP.NE.0) GO TO 210
93      C      *      *      *      MODIFY FOR SLOPING BOUNDARY CONDITIONS
94      200 DO 230 K=1,4
95          M=IX(N,K)
96          IF(CODE(M).GE.0.0) GO TO 230
97          CC=-CODE(M)
98          DX=COS(CC)
99          DY=SIN(CC)
100         L=2*K-1
101         DEN=P(L)*DX+P(L+1)*DY
102         P(L+1)=P(L+1)*DX-P(L)*DY
103         P(L)=DEN
104         DO 220 J=1,8,2
105         IF(J.EQ.L) GO TO 220
106         DEN=S(L,J)*DX+S(L+1,J)*DY
107         S(L+1,J)=S(L+1,J)*DX-S(L,J)*DY
108         S(L,J)=DEN

```

REAL TIME FORTRAN VER.E00 PAGE 3 DATE 83 08 23

```

109      S(J,L+1)=S(L+1,J)
110      S(J,L)=S(L,J)
111      DEN=S(L,J+1)*DX+S(L+1,J+1)*DY
112      S(L+1,J+1)=S(L+1,J+1)*DX-S(L,J+1)*DY
113      S(L,J+1)=DEN
114      S(J+1,L+1)=S(L+1,J+1)
115      S(J+1,L)=S(L,J+1)
116      220 CONTINUE
117      DEN=S(L,L)*DX*DX+2.0*S(L+1,L)*DX*DY+S(L+1,L+1)*DY*DY
118      S(L,L+1)=DX*DY*(S(L+1,L+1)-S(L,L))+S(L+1,L)*(DX*DX-DY*DY)
119      S(L+1,L+1)=S(L,L)*DY*DY-2.0*S(L+1,L)*DX*DY+S(L+1,L+1)*DX*DX
120      S(L,L)=DEN
121      S(L+1,L)=S(L,L+1)
122      230 CONTINUE
123      C      *      *      *      ADD STIFFNESS AND FORCE VECTORS
124      DO 240 I=1,4
125      240      LM(I)=2*IX(N,I)-2
126      DO 250 I=1,4
127      DO 250 K=1,2
128      II=LM(I)+K-KSHIFT
129      IF (II) 250,250,270
130      270      KK=2*I+K-2
131      B(II)=B(II)+P(KK)
132      DO 250 J=1,4
133      DO 250 L=1,2
134      JJ=LM(J)+L-II-KSHIFT+1
135      LL=2*J+L-2
136      IF (JJ) 250,250,260
137      260      A(JJ,II)=A(JJ,II)+S(KK,LL)
138      250 CONTINUE
139      210 CONTINUE
140      IF (ISTOP.NE.0) GO TO 390
141      C      *      *      *      ADD CONCENTRATED FORCES, MODIFY FOR DISPL B. C.
142      DO 350 N=NL,NM
143      K=2*N-KSHIFT-1
144      CC=CODE(N)
145      IF (CC.EQ.0.0) GO TO 340
146      IF (CC.EQ.1.0.OR.CC.EQ.11.0) CALL MODIFY(K,UX(2*N-1),NB,MBAND)
147      IF (CC.LT.0.0.OR.CC.EQ.10.0) CALL MODIFY(K+1,UX(2*N),NB,MBAND)
148      IF (CC.EQ.11.0) CALL MODIFY(K+1,UX(2*N),NB,MBAND)
149      340      B(K)=B(K)+UX(2*N-1)
150      B(K+1)=B(K+1)+UX(2*N)
151      350 CONTINUE
152      C      *      *      *      *      REDUCE BLOCK OF EQUATIONS
153      DO 370 N=1,ND
154      IF (A(1,N).EQ.0.0) GO TO 370
155      B(N)=B(N)/A(1,N)
156      DO 360 L=2,MBAND
157      IF (A(L,N).EQ.0.0) GO TO 360
158      CC=A(L,N)/A(1,N)
159      I=N+L-1
160      J=0
161      DO 380 K=L,MBAND
162      J=J+1

```

REAL TIME FORTRAN VER.E00 PAGE 4 DATE 83 08 23

```

163      380 A(J,I)=A(J,I)-CC*A(K,N)
164      B(I)=B(I)-A(L,N)*B(N)
165      A(L,N)=CC
166      360 CONTINUE
167      370 CONTINUE
168      390 IF(NM.EQ.NUMNP) GO TO 400
169      IF(ISTOP.NE.0) GO TO 6
170      C      *      *      WRITE BLOCK OF REDUCED EQUATIONS ON DISK
171      WRITE(11) (B(J), (A(I,J), I=1, MBAND), J=1, ND)
172      C      *      *      *      SHIFT BLOCK OF EQUATIONS UP FOR NEXT BLOCK
173      DO 410 N=1, ND
174      MM=ND+N
175      B(N)=B(MM)
176      B(MM)=0.0
177      DO 410 M=1, MBAND
178      A(M,N)=A(M,MM)
179      410 A(M,MM)=0.0
180      GO TO 6
181      400 IF(ISTOP.NE.0) GO TO 999
182      IF(IJK.NE.0) GO TO 405
183      ENDFILE 11
184      CALL F:ABST(@440, IER)
185      BACKSPACE 11
186      440 CONTINUE
187      IJK=1
188      C      *      *      *      *      BACK SUBSTITUTION
189      405 NU=ND*NUMBLK+1
190      415 DO 430 M=1, ND
191      N=ND-M+1
192      CC=B(N)
193      DO 420 K=2, MBAND
194      L=N+K-1
195      420 CC=CC-A(K,N)*B(L)
196      B(N)=CC
197      NM=N+ND
198      B(NM)=CC
199      NU=NU-1
200      430 UX(NU)=CC
201      NUMBLK=NUMBLK-1
202      IF(NUMBLK.LE.0) GO TO 500
203      BACKSPACE 11
204      READ(11) (B(J), (A(I,J), I=1, MBAND), J=1, ND)
205      BACKSPACE 11
206      GO TO 415
207      C      *      *      WRITE DISPLACEMENTS OF ELASTICITY NODES
208      500 WRITE(6,2000)
209      C      *      *      *      BOUNDARY ANGLE TRANSFORMATION
210      DO 510 N=1, NUMNP
211      IF(X(N).LT.0.0) GO TO 510
212      CC=-CODE(N)
213      IF(CC.LE.0.0) GO TO 520
214      DX=COS(CC)
215      DY=SIN(CC)
216      DEN=UX(2*N-1)*DX-UX(2*N)*DY

```

REAL TIME FORTRAN VER.E00 PAGE 5 DATE 83 08 23

```

217      UX(2*N)=UX(2*N-1)*DY+UX(2*N)*DX
218      UX(2*N-1)=DEN
219      520 WRITE(6,2001) N,X(N),Y(N),UX(2*N-1),UX(2*N)
220      510 CONTINUE
221      C      *      *      *      COMPUTE AND OUTPUT ELASTICITY ELEMENT STRESSES
222      MPRINT=0
223      DO 600 N=1,NUMEL
224      MT=IABS(IX(N,5))
225      C      *      *      *      FORM STRESS STRAIN RELATIONSHIP
226      CALL MODULI(N,I,J,K,L)
227      C      *      *      *      CALCULATION OF STRAINS AT CENTER NODAL POINT
228      IF(K.EQ.L) GO TO 610
229      F=0.25
230      NM=4
231      UK=F*(UX(2*I-1)+UX(2*J-1)+UX(2*K-1)+UX(2*L-1))
232      WK=F*(UX(2*I)+UX(2*J)+UX(2*K)+UX(2*L))
233      XK=F*(X(I)+X(J)+X(K)+X(L))
234      YK=F*(Y(I)+Y(J)+Y(K)+Y(L))
235      GO TO 620
236      610 XK=X(K)
237      YK=Y(K)
238      F=1.0
239      NM=1
240      K=2*K
241      UK=UX(K-1)
242      WK=UX(K)
243      620 CONTINUE
244      DO 630 NN=1,4
245      630 EPS(NN)=0.0
246      DO 640 NN=1,NM
247      M=NN+1
248      IF(NN.EQ.4) M=1
249      I=IX(N,NN)
250      J=IX(N,M)
251      AJ=X(J)-X(I)
252      AK=XK-X(I)
253      AT=AJ-AK
254      BJ=Y(J)-Y(I)
255      BK=YK-Y(I)
256      BT=BJ-BK
257      DT=AJ*BK-AK*BJ
258      DT=F/DT
259      I=2*I
260      J=2*J
261      EPS(1)=EPS(1)+DT*(BT*UX(I-1)+BK*UX(J-1)-BJ*UK)
262      EPS(3)=EPS(3)+DT*(-AT*UX(I)-AK*UX(J)+AJ*WK)
263      EPS(4)=EPS(4)+DT*(-AT*UX(I-1)+BT*UX(I)-AK*UX(J-1)+BK*UX(J)+
264      *AJ*UK-BJ*WK)
265      640 CONTINUE
266      C      *      *      *      CALCULATION OF STRESSES
267      DO 700 L=1,4
268      SIG(L)=0.0
269      DO 700 LL=1,4
270      700 SIG(L)=SIG(L)+C(L,LL)*EPS(LL)

```

REAL TIME FORTRAN VER.E00 PAGE 6 DATE 83 08 23

```

271 C      *      *      CALCULATE PRINCIPAL STRESSES AND STRAINS
272      DD=(EPS(1)+EPS(3))*0.5
273      DX=EPS(1)-EPS(3)
274      DR=SQRT(DX**2+EPS(4)**2)*0.5
275      EPS(5)=DD+DR
276      EPS(6)=DD-DR
277      IF(EPS(4).EQ.0.0.AND.DX.EQ.0.0) GO TO 800
278      EPS(7)=PII*ATAN2(EPS(4),DX)
279      CC=(SIG(1)+SIG(3))*0.5
280      CX=0.5*(SIG(1)-SIG(3))
281      CR=SQRT(CX*CX+SIG(4)**2)
282      SIG(5)=CC+CR
283      SIG(6)=CC-CR
284      SIG(7)=PII*ATAN2(SIG(4),CX)
285 C      *      *      STRESSES PARALLEL TO LINE J-K
286      I=IX(N,2)
287      J=IX(N,3)
288      ANGL=2.0*ATAN2(Y(J)-Y(I),X(J)-X(I))
289      CSA=COS(ANGL)
290      SNA=SIN(ANGL)
291      SIG(8)=-CX*CSA-SIG(4)*SNA+CC
292      EPS(8)=CX*SNA-SIG(4)*CSA
293      IF(MPRINT.GT.0) GO TO 810
294      MPRINT=16
295      WRITE(6,2002)
296      810 WRITE(6,2003) N,XK,YK,(SIG(I),I=1,8),MT,(EPS(I),I=1,8)
297      600 MPRINT=MPRINT-1
298      800 CONTINUE
299      WRITE(6,2004)
300      WRITE(6,4000)
301      WRITE(6,4000)
302      2000 FORMAT(1H1,2X,'NP',11X,'X1',11X,'X3',10X,'U1',10X,'U3'/)
303      2001 FORMAT(15,2F13.2,1P2E12.4)
304      2002 FORMAT(1H1,5H ELM ,5X,2HX1,6X,2HX3,4X,8H1-STRESS,4X,8H2-STRESS,
305      *4X,8H3-STRESS,3X,9H13-STRESS,2X,10HMAX-STRESS,2X,
306      *10HMIN-STRESS,2X,5HANGLE,3X,9HJK-STRESS/10X,8HMATERIAL,
307      *7X,8H1-STRAIN,4X,8H2-STRAIN,4X,8H3-STRAIN,3X,9H13-STRAIN,
308      *2X,10HMAX-STRAIN,2X,10HMIN-STRAIN,2X,5HANGLE,4X,8HJK-SHEAR)
309      2003 FORMAT(1H0,14,2F8.2,1P6E12.3,F7.2,1PE12.3/115,6X,1P6E12.3,
310      *F7.2,1PE12.3)
311      2004 FORMAT(/5X,'COMPUTATIONS COMPLETED')
312      3000 FORMAT(33X,'ZERO OR NEGATIVE AREA, ELEMENT=',14)
313      3001 FORMAT(10X,'MATERIAL TYPE NOT SPECIFIED FOR ELEMENT=',14)
314      4000 FORMAT(1H1)
315      999 STOP
316      END

```



REAL TIME FORTRAN VER.E00 PAGE 1 DATE 83 08 23

```

1      SUBROUTINE LOCATE(NPP,ISTOP,ACEL1,ACEL3,NB,MBAND)
2      DIMENSION IBC(50),JBC(50),PN(50),PT(50),XC(2),IN(2),XTYPE(25),
3      *NAME(40),ANG(1)
4      COMMON A(54,108),B(108)
5      COMMON/NPELD/E(7,10),RO(10),CODE(600),X(600),Y(600),
6      *UX(1200),IX(500,5),ANGLE(500),NUMNP,NUMEL,NUMPC
7      EQUIVALENCE (IBC,A(1,1)),(JBC,A(1,5)),(PN,A(1,7)),
8      *(PT,A(1,9)),(ANG,A(1,11))
9      DATA P1/0.017453/,MAXNP/600/,MAXEL/500/
10     C      *      *      *      READ AND PRINT CONTROL INFORMATION
11      READ(7,1000) NAME
12      WRITE(6,2000) NAME
13      READ(7,1001) NUMNP,NUMEL,NUMMAT,NUMPC,NPP,ACEL1,ACEL3
14      IF(NPP.EQ.1) GO TO 7
15      IF(NPP.EQ.2) GO TO 9
16      WRITE(6,2014)
17      ISTOP=1
18      GO TO 12
19      7 WRITE(6,2001)
20      GO TO 12
21      9 WRITE(6,2002)
22      12 IF(NUMNP.LE.MAXNP) GO TO 6
23      WRITE(6,3000) MAXNP
24      ISTOP=1
25      6 IF(NUMEL.LE.MAXEL) GO TO 8
26      WRITE(6,3001) MAXEL
27      ISTOP=1
28      RETURN
29      8 CONTINUE
30      WRITE(6,2003) NUMNP,NUMEL,NUMMAT,NUMPC,ACEL1,ACEL3
31     C      *      *      *      *      READ AND PRINT MATERIAL PROPERTIES
32      WRITE(6,2004)
33      DO 20 M=1,NUMMAT
34      READ(7,1002) MT,RO(MT),XTYPE
35      WRITE(6,2005) MT,XTYPE
36      READ(7,1003) (E(J,MT),J=1,7)
37      WRITE(6,2006) (E(J,MT),J=1,7),RO(MT)
38     C      *      *      *      *      MODIFY FOR PLANE STRESS IN LOCAL COORDINATES
39      IF(NPP.NE.2) GO TO 20
40      IF(E(4,MT).EQ.0.0) GO TO 20
41      EA=1.0/E(4,MT)
42      E(1,MT)=E(1,MT)-EA*(E(2,MT)**2)
43      E(3,MT)=E(3,MT)-EA*(E(2,MT)*E(5,MT))
44      E(6,MT)=E(6,MT)-EA*(E(5,MT)**2)
45      E(2,MT)=0.0
46      E(4,MT)=0.0
47      E(5,MT)=0.0
48      WRITE(6,2009)
49      WRITE(6,2006) (E(J,MT),J=1,7),RO(MT)
50      20 CONTINUE
51     C      *      *      *      *      READ AND PRINT NODAL DATA
52      N=0
53      WRITE(6,2007)
54      DO 95 L=1,NUMNP

```

REAL TIME FORTRAN VER.E00 PAGE 2 DATE 83 08 23

```

55      IF (L-N) 70,85,55
56      55 READ(7,1004) N, CODE(N), X(N), Y(N), UX(2*N-1), UX(2*N), ANG(N)
57      CODE(N)=ABS(CODE(N))
58      DV=X(N)
59      DU=Y(N)
60      IF (L-N) 60,85,100
61      60 DZ=N-L+1
62      DX=(X(N)-X(L-1))/DZ
63      DY=(Y(N)-Y(L-1))/DZ
64      70 CODE(L)=0.0
65      IF (CODE(N).EQ.CODE(L-1)) CODE(L)=CODE(L-1)
66      IF (ANG(N).EQ.ANG(L-1)) ANG(L)=ANG(L-1)
67      UX(2*L-1)=0.0
68      UX(2*L)=0.0
69      X(L)=X(L-1)+DX
70      Y(L)=Y(L-1)+DY
71      85 WRITE(6,2008) L, CODE(L), X(L), Y(L), UX(2*L-1), UX(2*L), ANG(L)
72      IF (ANG(L).NE.0.0) CODE(L)=-ANG(L)*PI
73      95 CONTINUE
74      GO TO 110
75      100 WRITE(6,3002) N
76      ISTOP=1
77      110 CONTINUE
78      C      *      *      *      * READ AND PRINT ELEMENT PROPERTIES
79      N=0
80      WRITE(6,2010)
81      130 READ(7,1005) M, (IX(M,I), I=1,5), ANGLE(M)
82      140 N=N+1
83      IF (M.LE.N) GO TO 160
84      IX(N,1)=IX(N-1,1)+1
85      IX(N,2)=IX(N-1,2)+1
86      IX(N,3)=IX(N-1,3)+1
87      IX(N,4)=IX(N-1,4)+1
88      IX(N,5)=IX(N-1,5)
89      ANGLE(N)=ANGLE(N-1)
90      160 WRITE(6,2011) N, (IX(N,I), I=1,5), ANGLE(N)
91      IF (M-N) 185,180,140
92      180 IF (NUMEL-N) 185,190,130
93      185 WRITE(6,3003) N
94      ISTOP=1
95      190 CONTINUE
96      C      *      *      *      * READ AND PRINT PRESSURE BOUNDARY CONDITIONS
97      IF (NUMPC.EQ.0) GO TO 310
98      WRITE(6,2012)
99      DO 300 L=1, NUMPC
100     READ(7,1006) IBC(L), JBC(L), PN(L), PT(L)
101     300 WRITE(6,2013) IBC(L), JBC(L), PN(L), PT(L)
102     310 CONTINUE
103     C      *      *      * DETERMINE BANDWIDTH AND COMPUTE SURFACE INTEGRALS
104     ND=2*NB
105     MB=0
106     DO 340 N=1, NUMEL
107     ANGLE(N)=PI*ANGLE(N)
108     DO 340 I=1, 4

```

REAL TIME FORTRAN VER.E00 PAGE 3 DATE 83 08 23

```

109      IF (NUMPC.LE.0) GO TO 240
110      J=I+1
111      IF (I.EQ.4) J=1
112      K=IX(N,I)
113      L=IX(N,J)
114      DO 230 MM=1,NUMPC
115      IF (K.NE.IBC(MM).OR.L.NE.JBC(MM)) GO TO 230
116      IBC(MM)=0
117      XC(1)=CODE(K)
118      XC(2)=CODE(L)
119      IN(1)=K
120      IN(2)=L
121      DX=X(L)-X(K)
122      DY=Y(L)-Y(K)
123      FX=0.5*(PT(MM)*DX-PN(MM)*DY)
124      FY=0.5*(PT(MM)*DY+PN(MM)*DX)
125      DO 225 K=1,2
126      L=IN(K)
127      C=XC(K)
128      IF (C.GE.0.0) GO TO 205
129      UX(2*L-1)=UX(2*L-1)+FX*COS(C)-FY*SIN(C)
130      GO TO 225
131      205 IF (C.EQ.1.0.OR.C.EQ.11.0) GO TO 210
132      UX(2*L-1)=UX(2*L-1)+FX
133      210 IF (C.EQ.10.0.OR.C.EQ.11.0) GO TO 225
134      UX(2*L)=UX(2*L)+FY
135      225 CONTINUE
136      230 CONTINUE
137      240 DO 325 J=1,4
138      K=IABS(IX(N,I)-IX(N,J))
139      325 IF (K.GT.MB) MB=K
140      340 CONTINUE
141      IF (NUMPC.EQ.0) GO TO 355
142      DO 350 MM=1,NUMPC
143      IF (IBC(MM).EQ.0) GO TO 350
144      WRITE(6,3004) MM
145      ISTOP=1
146      350 CONTINUE
147      355 MBAND=2*MB+2
148      WRITE(6,2015) MBAND
149      IF (MBAND.LE.ND) GO TO 360
150      WRITE(6,3005) MBAND
151      ISTOP=1
152      360 RETURN
153      1000 FORMAT(40A2)
154      1001 FORMAT(5I5,2F10.0)
155      1002 FORMAT(15,F10.0,25A2)
156      1003 FORMAT(7E10.4)
157      1004 FORMAT(15,F5.0,5F10.0)
158      1005 FORMAT(6I5,F10.0)
159      1006 FORMAT(2I5,2F10.0)
160      2000 FORMAT(1H1,5X,40A2)
161      2001 FORMAT(1H0,20X,'PLANE STRAIN PROBLEM')
162      2002 FORMAT(1H0,20X,'PLANE STRESS PROBLEM')

```

REAL TIME FORTRAN VER.E00 PAGE 4 DATE 83 08 23

```

163 2003 FORMAT(1H0,4X,'NUMBER OF NODAL POINTS-----',I4/
164      *5X,'NUMBER OF ELEMENTS-----',I4/
165      *5X,'NUMBER OF DIFFERENT MATERIALS---',I4/
166      *5X,'NUMBER OF PRES/SHEAR CONDITIONS-',I4/
167      *5X,'X1 ACCELERATION-----',1PE12.4/
168      *5X,'X3 ACCELERATION-----',1PE12.4/)
169 2004 FORMAT(1H1,20X,'MATERIAL DATA')
170 2005 FORMAT(1H0,2X,I2,10X,25A2)
171 2006 FORMAT(7X,'C11=',1PE10.2,2X,'C12=',E10.2,2X,'C13=',E10.2,2X,
172      *'C22=',E10.2/7X,'C23=',E10.2,2X,'C33=',E10.2,2X,'C44=',
173      *E10.2,2X,'DENSITY=',E10.2)
174 2007 FORMAT(1H1,3X,'NODE PNT',8X,'CODE',4X,'X1-COORD',4X,
175      *'X3-COORD',2X,'X1-LD OR DISP',2X,'X3-LD OR DISP',9X,'ANGLE'/)
176 2008 FORMAT(1I2,F12.0,2F12.4,1P3E15.4)
177 2009 FORMAT(30X,'PLANE STRESS REDUCTION OF MATR. COEF.')

```

REAL TIME FORTRAN VER.E00 PAGE 1 DATE 83 08 23

```

1      SUBROUTINE TRISTF (II,JJ,KK,NPP,ISTOP,COMM,AM1,AM3)
2      DIMENSION F(6,10),H(6,10),DD(3,3),LM(3),D(6,6),XI(3)
3      COMMON/QADTRI/XXX(5),YYY(5),C(4,4),S(10,10),P(10)
4      DATA D/36*0.0/
5      LM(1)=II
6      LM(2)=JJ
7      LM(3)=KK
8      C11=XXX(II)
9      C12=XXX(JJ)
10     C13=XXX(KK)
11     C21=YYY(II)
12     C22=YYY(JJ)
13     C23=YYY(KK)
14     COMM=C12*(C23-C21)+C11*(C22-C23)+C13*(C21-C22)
15     IF (COMM.LE.0.0.OR.ISTOP.NE.0) RETURN
16     C      *      *      *      *      *      *      * FORM INTEGRAL GT*C*G
17     F(1,4)=(C11+C12)/2.0
18     F(1,5)=(C12+C13)/2.0
19     F(1,6)=(C13+C11)/2.0
20     F(2,4)=(C21+C22)/2.0
21     F(2,5)=(C22+C23)/2.0
22     F(2,6)=(C23+C21)/2.0
23     GO TO (30,10),NPP
24     10 DO 20 I=4,6
25     20 F(3,I)=1.0
26     GO TO 40
27     30 DO 35 I=4,6
28     35 F(3,I)=F(1,I)
29     40 DO 50 I=1,3
30     50 XI(I)=0.0
31     DO 100 I=4,6
32     XI(1)=XI(1)+F(3,I)
33     XI(2)=XI(2)+F(3,I)*F(1,I)
34     XI(3)=XI(3)+F(3,I)*F(2,I)
35     100 CONTINUE
36     DO 108 I=1,10
37     DO 108 J=1,6
38     H(J,I)=0.0
39     108 F(J,I)=0.0
40     D(2,6)=XI(1)*C(1,3)*COMM/6.0
41     D(3,5)=XI(1)*C(4,4)*COMM/6.0
42     D(5,5)=XI(1)*C(4,4)*COMM/6.0
43     D(5,6)=XI(1)*C(3,4)*COMM/6.0
44     D(6,6)=XI(1)*C(3,3)*COMM/6.0
45     D(3,6)=XI(1)*C(3,4)*COMM/6.0
46     D(2,2)=XI(1)*C(1,1)*COMM/6.0
47     D(2,3)=XI(1)*C(1,4)*COMM/6.0
48     D(2,5)=XI(1)*C(1,4)*COMM/6.0
49     D(3,3)=XI(1)*C(4,4)*COMM/6.0
50     DO 110 I=2,6
51     DO 110 J=1,1
52     110 D(I,J)=D(J,I)
53     C      *      *      *      *      * FORM COEF-DISPL TRANSFORMATION MATRIX
54     DD(1,1)=(C12*C23-C13*C22)/COMM

```

REAL TIME FORTRAN VER.E00 PAGE 2 DATE 83 08 23

```

55      DD(1,2)=(C13*C21-C11*C23)/COMM
56      DD(1,3)=(C11*C22-C12*C21)/COMM
57      DD(2,1)=(C22-C23)/COMM
58      DD(2,2)=(C23-C21)/COMM
59      DD(2,3)=(C21-C22)/COMM
60      DD(3,1)=(C13-C12)/COMM
61      DD(3,2)=(C11-C13)/COMM
62      DD(3,3)=(C12-C11)/COMM
63      DO 120 I=1,3
64      J=2*LM(I)-1
65      H(1,J)=DD(1,I)
66      H(2,J)=DD(2,I)
67      H(3,J)=DD(3,I)
68      H(4,J+1)=DD(1,I)
69      H(5,J+1)=DD(2,I)
70      120 H(6,J+1)=DD(3,I)
71      C      *      *      *      * FORM ELEMENT STIFFNESS MATRIX HT*D*H
72      DO 130 J=1,10
73      DO 130 K=1,6
74      IF(H(K,J).EQ.0.0) GO TO 130
75      DO 125 I=1,6
76      125 F(I,J)=F(I,J)+D(I,K)*H(K,J)
77      130 CONTINUE
78      DO 140 I=1,10
79      DO 140 K=1,6
80      IF(H(K,I).EQ.0.0) GO TO 140
81      DO 135 J=1,10
82      135 S(I,J)=S(I,J)+H(K,I)*F(K,J)
83      140 CONTINUE
84      C      *      *      *      * FORM BODY FORCE VECTOR
85      F(1,1)=AM1*XI(1)*COMM/6.0
86      F(2,1)=AM1*XI(2)*COMM/6.0
87      F(3,1)=AM1*XI(3)*COMM/6.0
88      F(4,1)=AM3*XI(1)*COMM/6.0
89      F(5,1)=AM3*XI(2)*COMM/6.0
90      F(6,1)=AM3*XI(3)*COMM/6.0
91      DO 160 I=1,10
92      DO 160 K=1,6
93      160 P(I)=P(I)+H(K,I)*F(K,1)
94      RETURN
95      END

```

REAL TIME FORTRAN VER.E00 PAGE 1 DATE 83 08 23

```

1      SUBROUTINE MODULI(N,I,J,K,L)
2      COMMON/NPELD/E(7,10),RO(10),CODE(600),X(600),Y(600),
3      *UX(1200),IX(500,5),ANGLE(500),NUMNP,NUMEL,NUMPC
4      COMMON/GADTRI/XXX(5),YYY(5),C(4,4),S(10,10),P(10)
5      C      *      *      *      *      *      *      *      *      *      *      *      *      *      *      *      *
6      DO 10 I=1,4
7      DO 10 J=1,4
8      10  C(I,J)=0.0
9      I=IX(N,1)
10     J=IX(N,2)
11     K=IX(N,3)
12     L=IX(N,4)
13     MT=IABS(IX(N,5))
14     C11=E(1,MT)
15     C12=E(2,MT)
16     C13=E(3,MT)
17     C22=E(4,MT)
18     C23=E(5,MT)
19     C33=E(6,MT)
20     C44=E(7,MT)
21     C      *      *      *      *      *      *      *      *      *      *      *      *      *      *      *      *
22     CS=COS(ANGLE(N))
23     SN=SIN(ANGLE(N))
24     CS2=CS**2
25     SN2=SN**2
26     CS4=CS2**2
27     SN4=SN2**2
28     DEN=2.0*(C13+2.0*C44)*CS2*SN2
29     C(1,1)=C11*CS4+C33*SN4+DEN
30     C(3,3)=C33*CS4+C11*SN4+DEN
31     C(1,3)=C13*(CS4+SN4)+(C11+C33-4.0*C44)*CS2*SN2
32     DEN=(C13+2.0*C44)*(CS2-SN2)
33     C(1,4)=(C11*CS2-C33*SN2-DEN)*CS*SN
34     C(3,4)=(C11*SN2-C33*CS2+DEN)*CS*SN
35     C(4,4)=C44*(CS2-SN2)**2+(C11-2.0*C13+C33)*CS2*SN2
36     C(2,2)=C22
37     C(1,2)=C12*CS2+C23*SN2
38     C(2,3)=C23*CS2+C12*SN2
39     C(2,4)=(C12-C23)*CS*SN
40     C(2,1)=C(1,2)
41     C(3,1)=C(1,3)
42     C(4,2)=C(2,4)
43     C(3,2)=C(2,3)
44     C(4,1)=C(1,4)
45     C(4,3)=C(3,4)
46     RETURN
47     END

```

REAL TIME FORTRAN VER.E00 PAGE 1 DATE 83 08 23

```
1      SUBROUTINE MODIFY(N,X,NB,MBAND)
2      COMMON A(54,108),B(108)
3      ND2=4*NB
4      DO 250 M=2,MBAND
5      K=N-M+1
6      IF(K.LE.0) GO TO 240
7      B(K)=B(K)-A(M,K)*X
8      A(M,K)=0.0
9      240 K=N+M-1
10     IF(K.GT.ND2) GO TO 250
11     B(K)=B(K)-A(M,N)*X
12     A(M,N)=0.0
13     250 CONTINUE
14     A(1,N)=0.0
15     B(N)=0.0
16     RETURN
17     END
```

(Manuscript prepared September 1983, Manuscript received February 13, 1984)



## コンピュータープログラム・LOPE

セオドル・イー・ラング\*・沼野夏生・阿部 修\*\*

国立防災科学技術センター新庄支所

弾性問題やそれに類する問題は、有限要素法を用いた本プログラム（LOPE、この略称は局所直交異方性をもつ弾性体の平面問題を意味する）の適用によって、より容易に解くことができる。本プログラムの直接の適用対象は、二次元弾性問題であり、そこでは材料の直交異方性、弾性体の表面や内部への荷重、拘束的境界条件を考慮することができる。さらに、本プログラムのアルゴリズムは定常流（ポテンシャル流）の問題、例えば理想流体の流れ、粘弾性定常クリープ現象、多孔質の媒体中の流れ、熱伝達などの解析にも適用できる。本プログラムにおける基本的要素は、ひずみが一定の三角形であるが、これを重ねることにより四辺形の要素を定義することもできる。本プログラムは一連の代数方程式を解くためにガウスの消去法を用いており、大規模な問題をさほど容量の大きくないコンピューターシステムを用いて解くことを可能にするために、これらの方程式はマトリックス分割の手法によって処理されている。すなわち、マトリックスの分割された部分を補助記憶装置に一時的に格納しつつ順次演算することにより、主記憶容量の制約を回避している。こうした特徴を持ったため、本プログラムは国立防災科学技術センター新庄支所のメルコム70コンピューターシステムで稼動することが可能となり、主記憶容量を超過する大規模な問題を解くのに利用されている。本報告には原始プログラムリストのほか、入力フォーマットの記述法と、各種のオプションの働きを確認するためのいくつかの例題を掲載した。

\* 昭和58年度科学技術庁外国人研究者招へい制度で来日、アメリカ・モンタナ州立大学工学部土木工学科・機械力学科教授、\*\* 雪害防災研究室